

Rail maintenance and its impact on Squat mitigation

ICRI Webinar, 30/06/2020

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- A history of Squats
- The Squat staircase concept
- Maintenance technologies
- Rail maintenance and Squats
- Summary



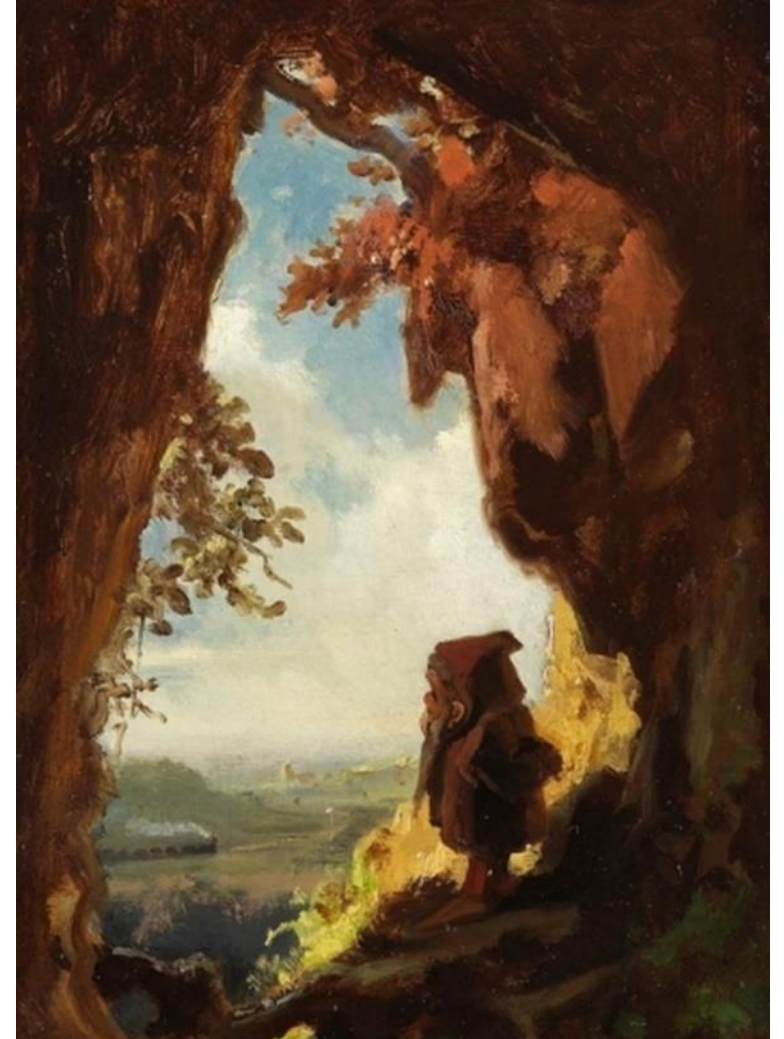
- In Japan observed since 1950s on Shinkansen high speed tracks – dark spots
- In France and UK since the late 1970ies
- Massed renaissance in Europe and other continents since the late 1990s



Photo: Wikipedia, CC BY-SA 4.0, © Alpsdake

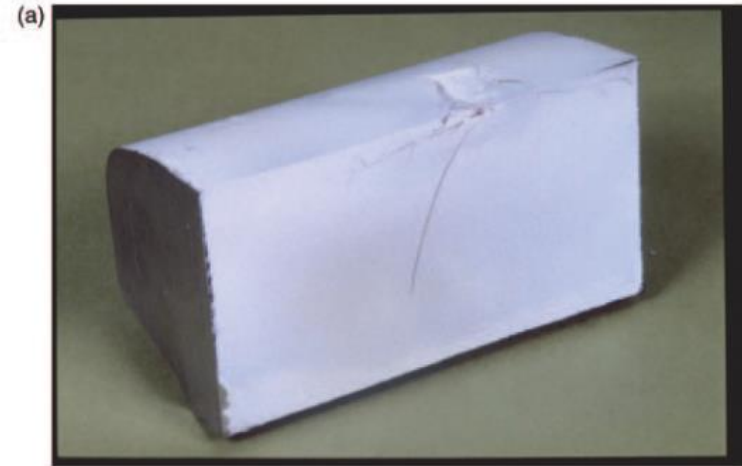


- Verb: to squat
- Definition: crouch or sit with one's knees bent and one's heels close to or touching one's buttocks or the back of one's thighs.
- British Railway employees defined the name
 - As if a Gnome was squatting on the rail and left a mark
- Proof of interest of Gnomes on railways
 - Painting by Carl Spitzweg, ca. 1848
 - “Gnome watching railway train”



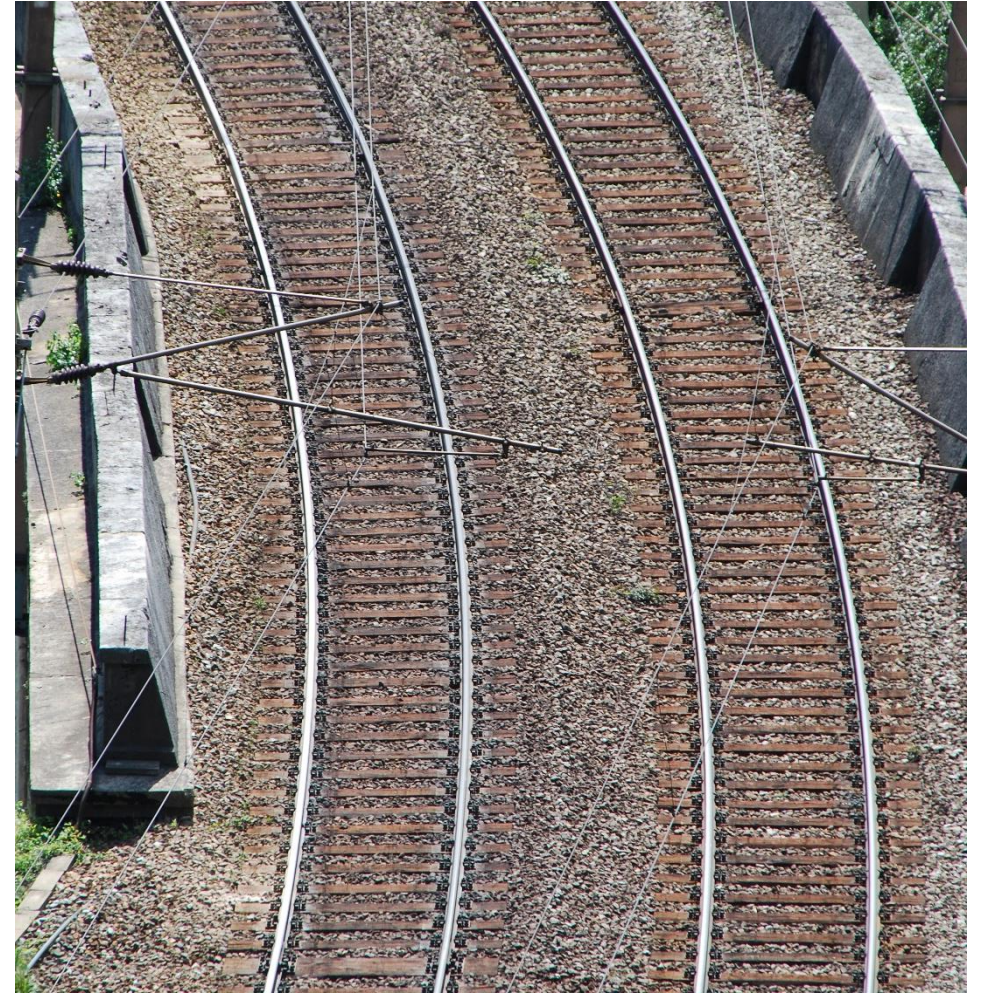
Cropped painting by Carl Spitzweg, 1848, public domain

- Characteristics
 - Heavily sheared rail surface
 - Crack initiation and growth by ratcheting (RCF)
 - Initiation after a few 10s of MGT
 - Slow growth (within 100+ MGT) to full size
- Straight track and shallow curves
- Can result in rail break



Photos taken from: S.L. Grassie: Squats and squat-type defects in rails: the understanding to date. In Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit, 2012, Volume 226, Issue 3, 235 – 242
Original: British Rail Research, CO Frederick

- Introduction of cyclic-preventive maintenance
 - Removal of damaged layer
- Introduction of higher strength rail grades
 - From R200/R220 to R260
 - Less plastic deformation and damage



- Massed re-appearance in 90ies
- Superficial similarity to “old” Squats
- Characteristics:
 - Almost no plastic deformation
 - Formation within 10MGT or less
 - Low wear conditions
 - No directly related rail breaks reported
- Preventive rail maintenance strategies of limited mitigation success
- Also called Stud or Squat Type Defect

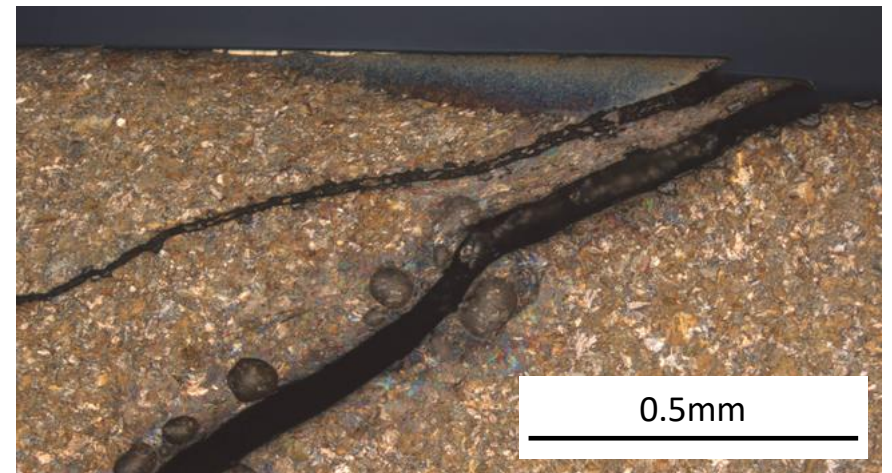
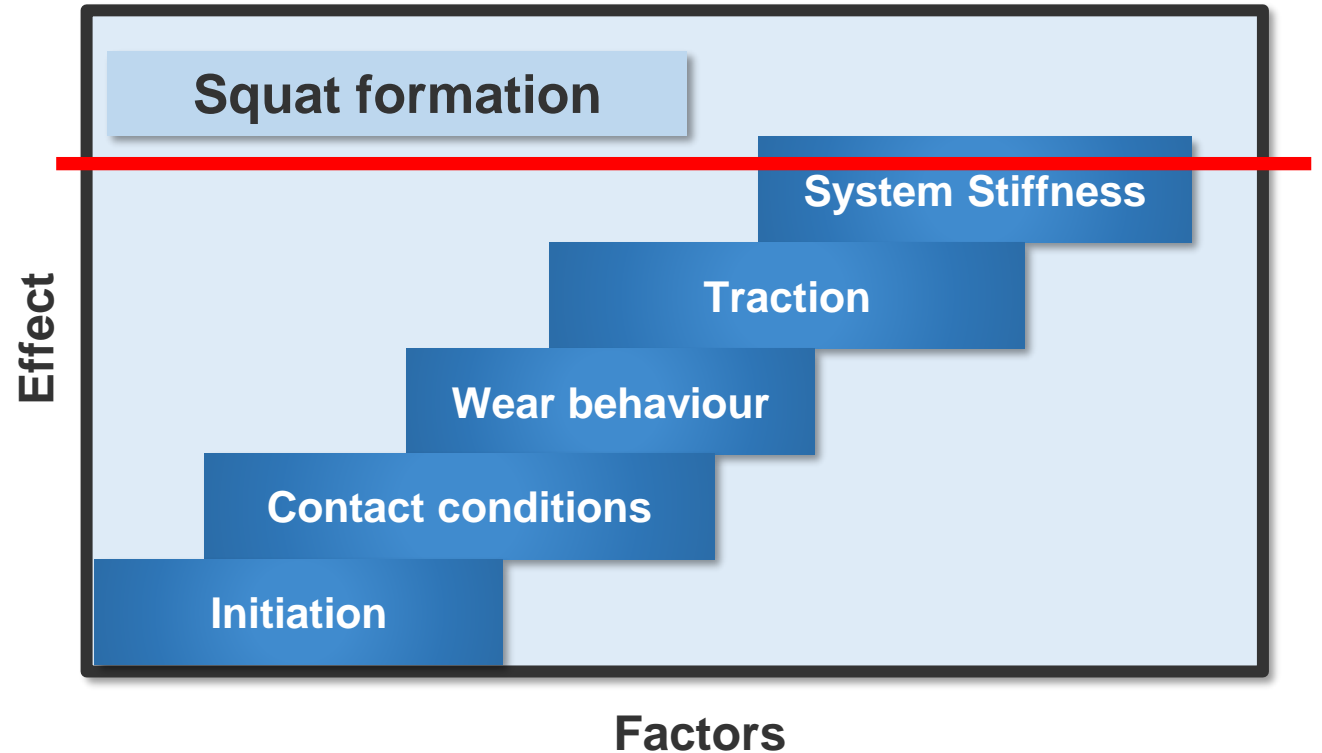


Photo by voestalpine

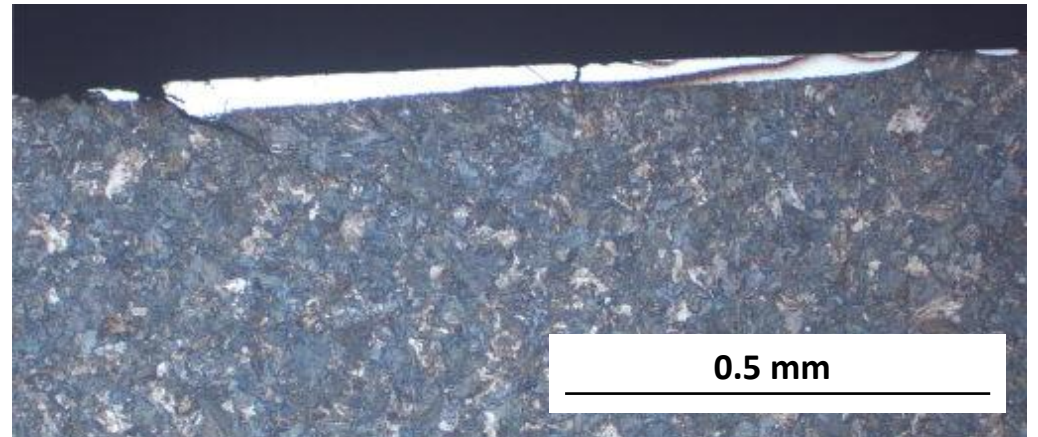
- Development of Squat Damage Staircase Concept
- Complex and multi-factor problem



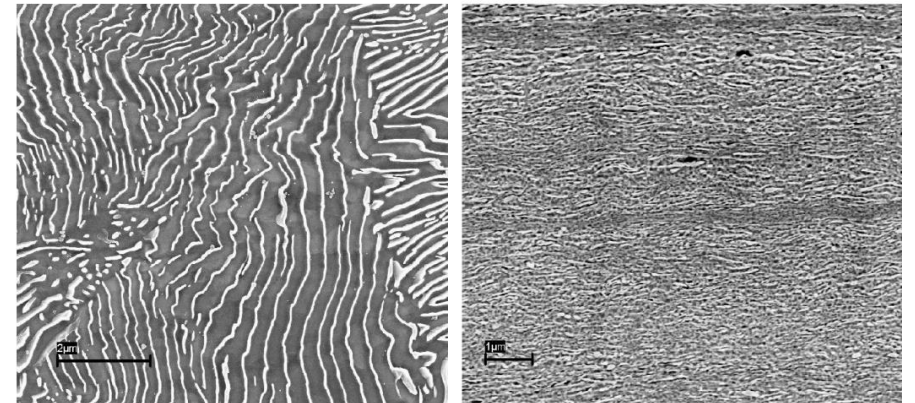
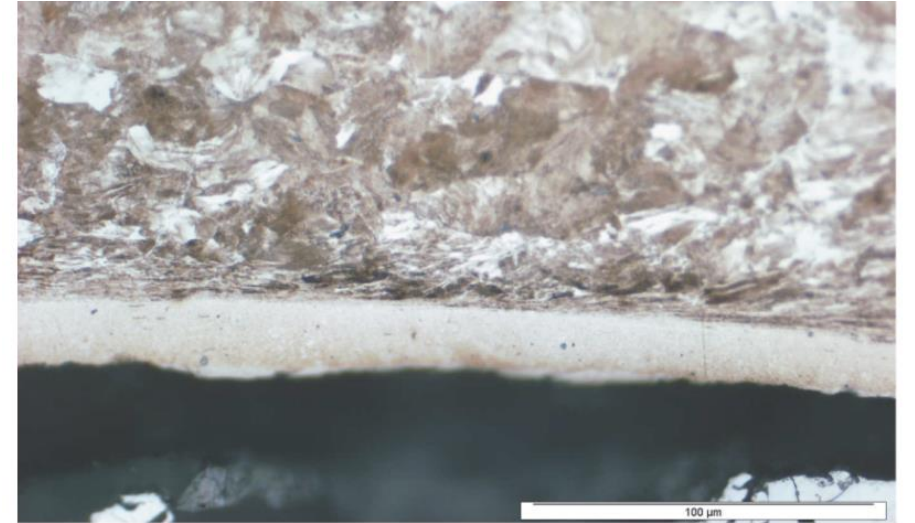
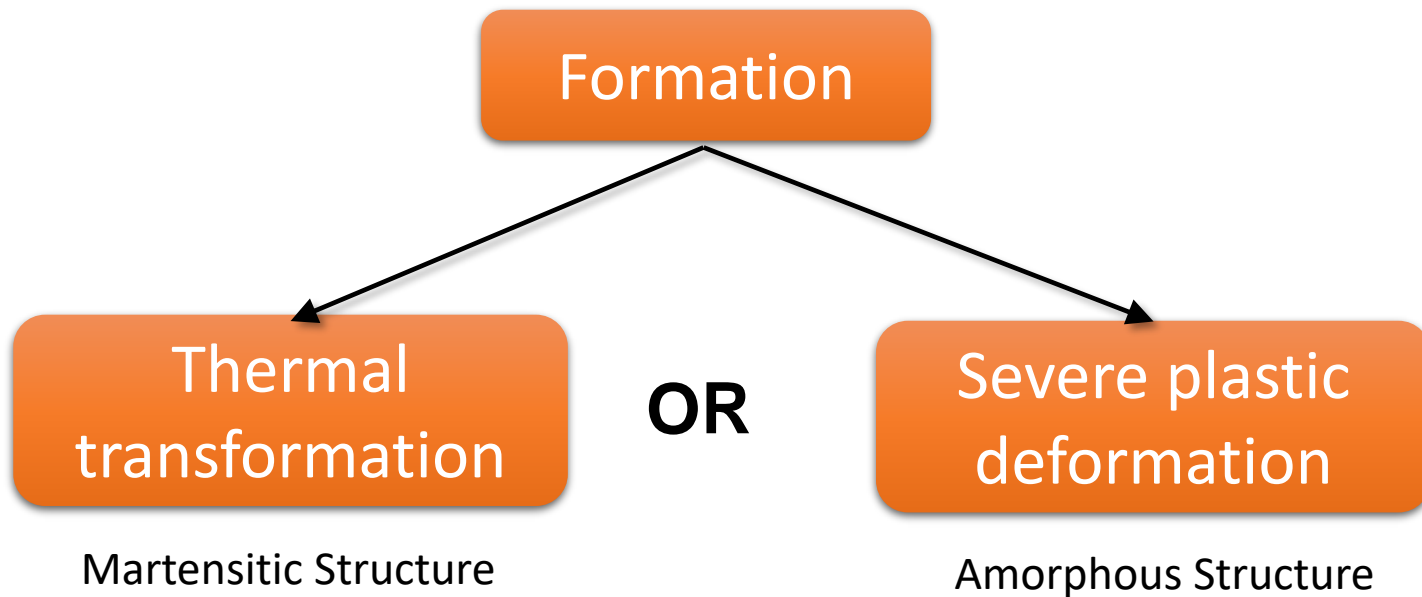
Squat Damage Staircase Concept

Original version: Jörg, A.; Stock, R.; Scheriau, S.; Brantner, H.P.; Knoll, B.; Mach, M.; Daves, W.: The squat condition of rail materials – a novel approach, in: Proceedings of CM 2015, Colorado Springs.

- Initiation points necessary for Squats
 - Imprints
 - Corrugation
 - Welds
 - Head Checks
 - Surface structure after rail grinding
 - *White Etching Layers / martensitic layers*
 - Rail surface deviation
- Right order of magnitude
- Direct or indirect initiation point



- Area that is not etched by 3% Nital Acid will appear white in light microscope
- Hard and brittle layers



Photos: Florian Wetscher, Effect of Large Shear Deformation on Rail Steels and Pure Metals, Doctoral Thesis, 2006, University of Leoben

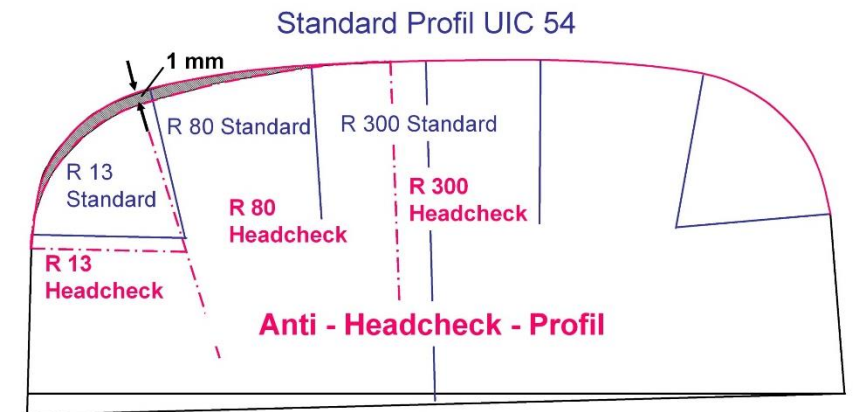
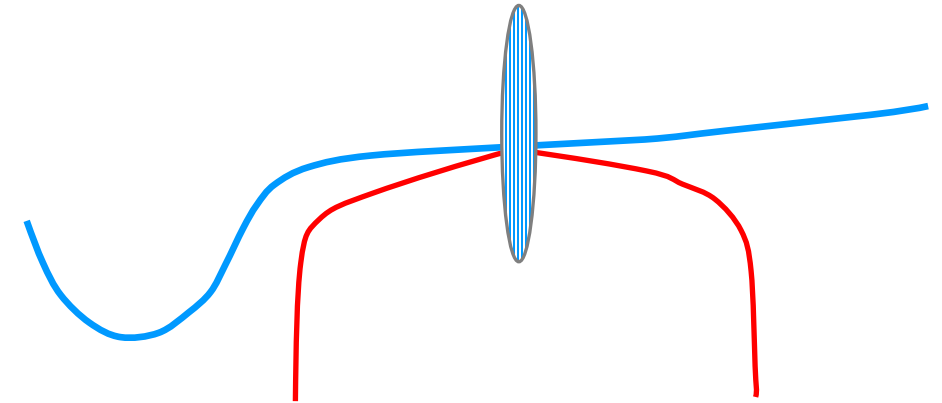
- Origin
 - vehicle traction (accelerating and braking)
 - rail grinding activities
- WEL are widely found in track – initiation point for Squats?

Multiple open questions:

- Only a certain % of WEL contribute to Squats
- What is the characteristic of a Squat-WEL (thickness, structure, interface to base material, wear behaviour,...)?

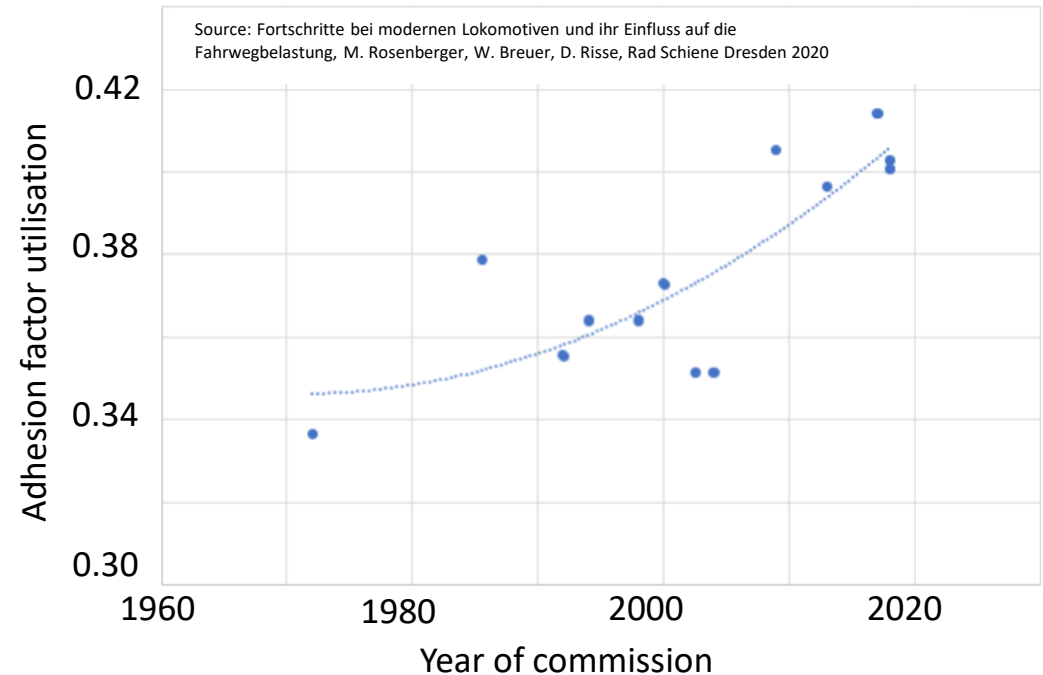
Other influencing factors: Squat Staircase Concept

- Narrow contact patch – high stress conditions
 - Favor formation of Squats
 - Wear resistant grades keep unfavorable contact condition over longer time period
- Implementation of Anti-Head Check profiles
 - Gauge corner relieve by undercutting
 - Shifting contact to concentrated area on TOR
 - AHC might/will favor Squats
- Low wear conditions and unfavorable profile combinations will favor Squats

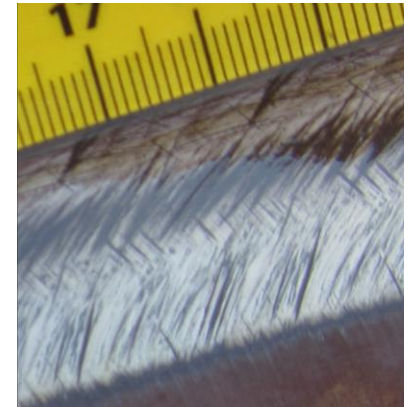
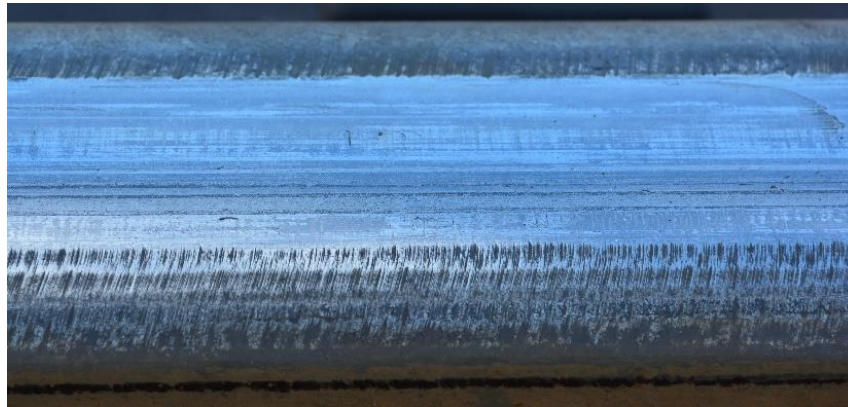


R. Stock, W. Schöch: Keeping Rolling Contact Fatigue under Control - Steel Grade Selection & Appropriate Rail Maintenance. WRI 2011 Conference, Chicago

- Squats at sites with high tractive forces
 - Signals, train stations and open track -> WEL
- Since 1990s change from DC to AC traction
 - AC traction allows controlled operations with high traction forces at higher slips
 - Higher adhesion utilisation
- Continuously increasing traction power



- Traction control systems (TCS) / wheel slip prevention systems (WSP)
 - Aggressiveness of TCS will impact damage formation
 - Adhesion recovery strategies
 - Drive oscillations
 - Regular traction marks on the rail surface (WEL)
- Distributed power for EMU/DMU



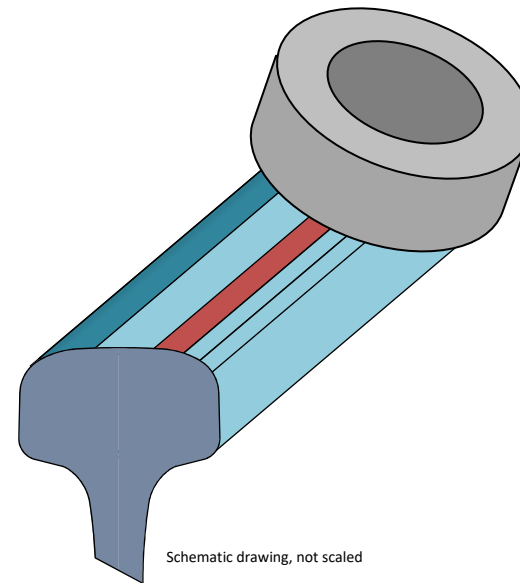
- Empirical evidence was found that “stiff” rail-wheel systems will favor Squat formation
 - Stiff suspension systems of vehicles
 - Stiff track constructions (stiff rail pads, concrete sleepers, slab track)
- Increased dynamic forces
 - Possible interaction with traction systems to favor wheel slip events
- Increased rotational boogie stiffness during curving
 - Passenger trains need to run stable at high speeds
 - Increased lateral forces and lateral creep
- Quantification difficult



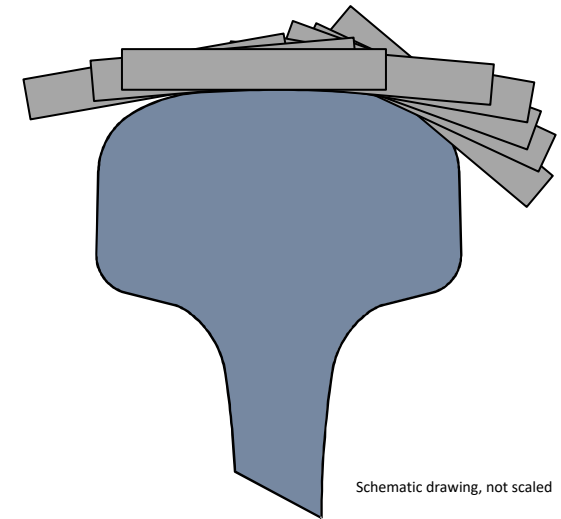
- Abrasive process with rotating grinding stones
- Flexible profile adjustment through stone alignment
- Variable machine size (4-120 stones)
- Process speed up to 15 km/h
- Capable of treating mainline track and switches (dedicated machines)



Photo by Glucke, Wikipedia, CC BY-SA 3.0



Schematic drawing, not scaled



Schematic drawing, not scaled

- Despite preventive maintenance strategies squat defects still persistent
- Removal of cap and extended spalling
- Repeatedly high temperature input above 723°C
- Formation of WEL layers
- Creating of characteristic surface roughness and morphology

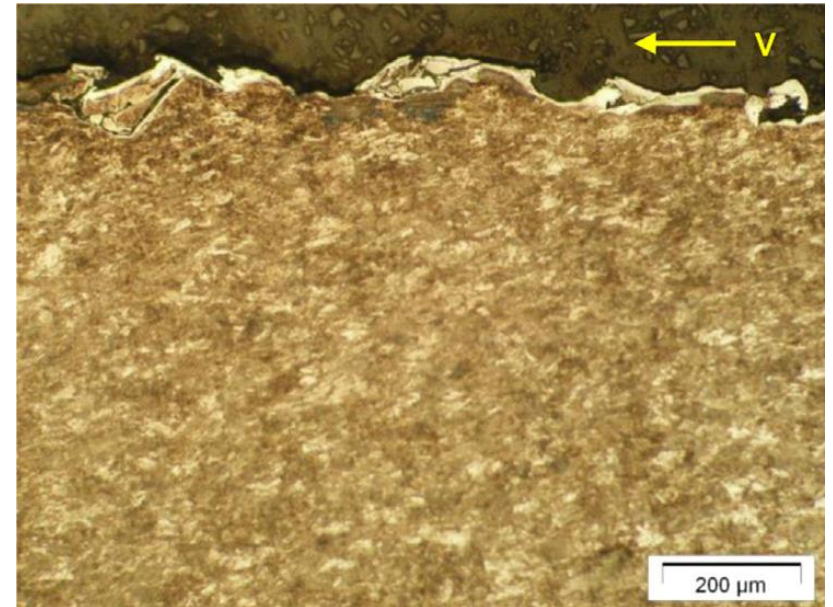
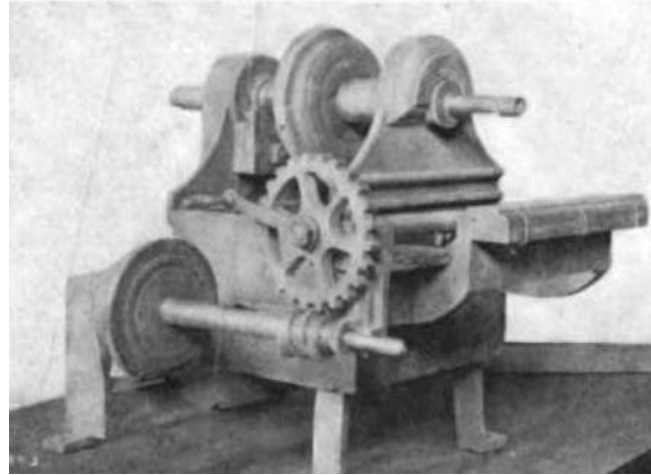


Photo: M. Steenbergen. Rolling contact fatigue in relation to rail grinding, Wear 356-357 (2016) 110-121

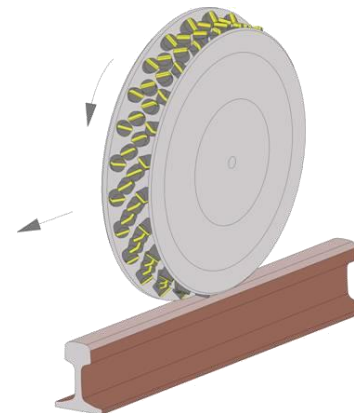
- Milling of work pieces since 19th century
- Non - abrasive rotary cutting process
 - Chips cut out of surface
 - High quality surface finish
 - High precision geometry
- High precision CNC machine upside-down on a locomotive
- Mainline and switch treatment with same machine



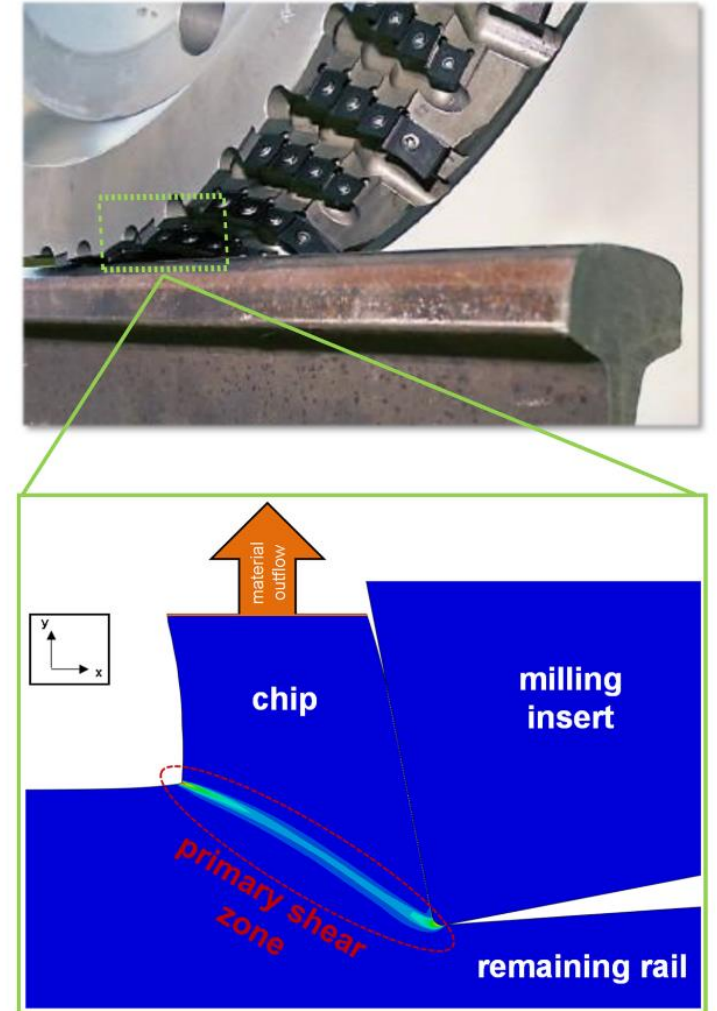
Milling Machine, 1818, wikipedia



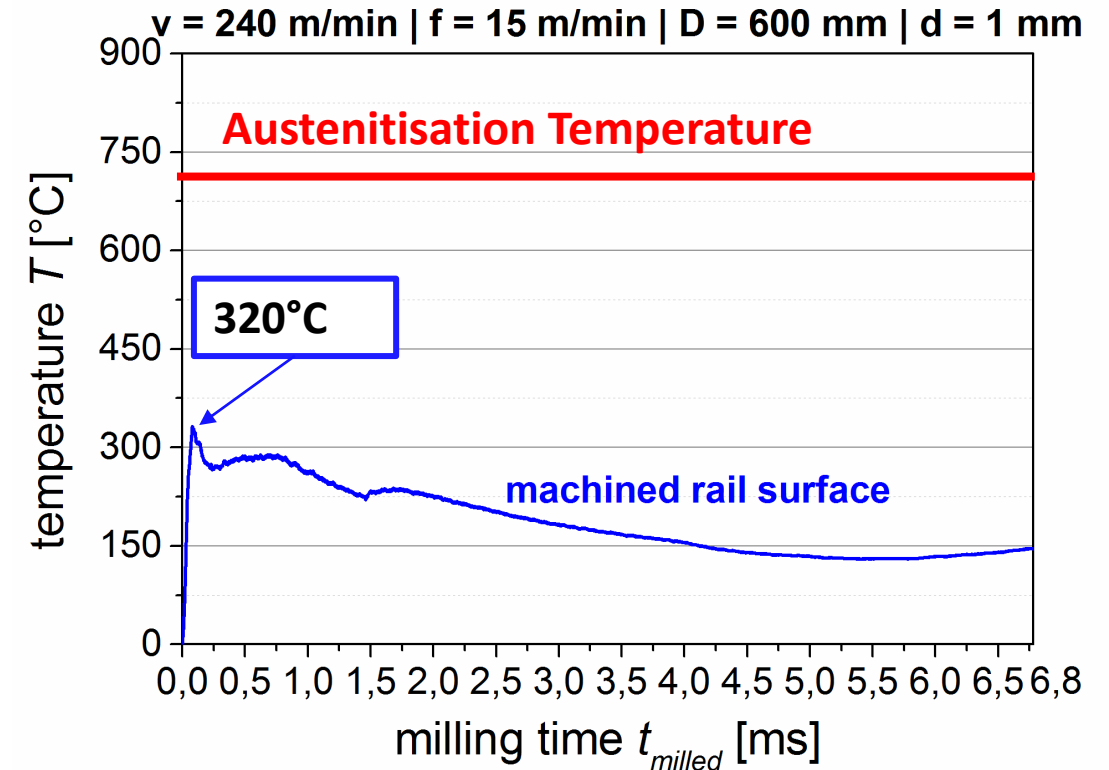
Rail Milling Machine SF02, 2016, LINMAG



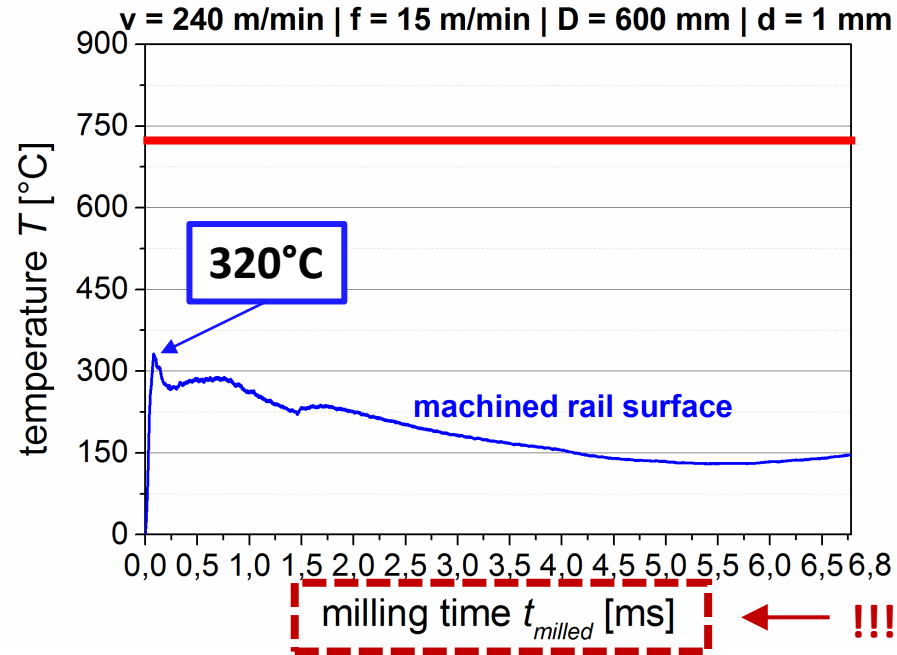
- Collaboration with Materials Center Leoben and University of Leoben in Austria
- Simulation of Milling Process
 - 3D and 2D simulation model developed
 - Simulation of complete process
- Simulation of material removal and chip development
- Detailed analysis of temperature development during milling process



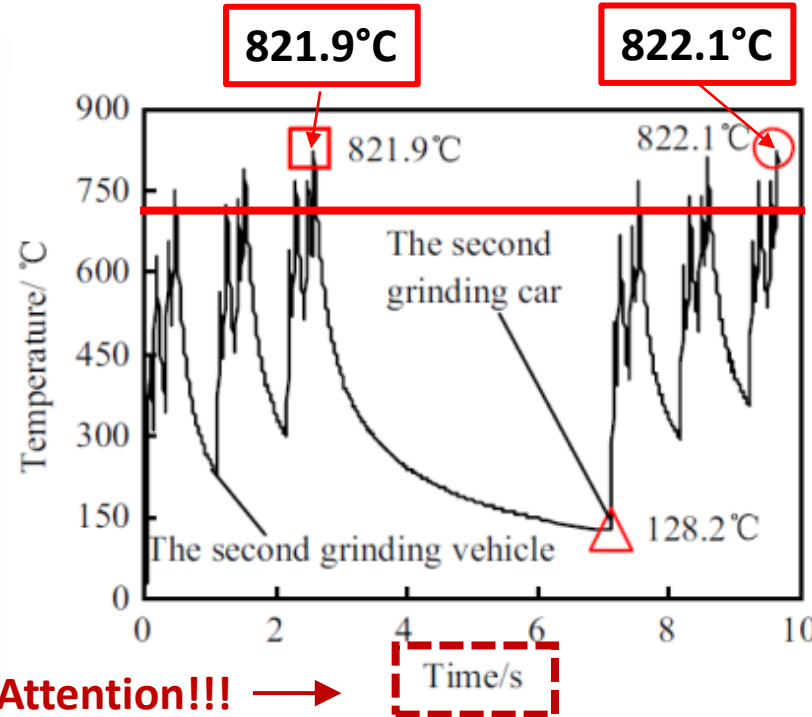
- Simulation of the milling process (2D)
- Process heat flows into milling insert and chip
- Rail temperature stays well below austenitizing temperature during and after milling
 - Temperature threshold for material transformations



milling



grinding



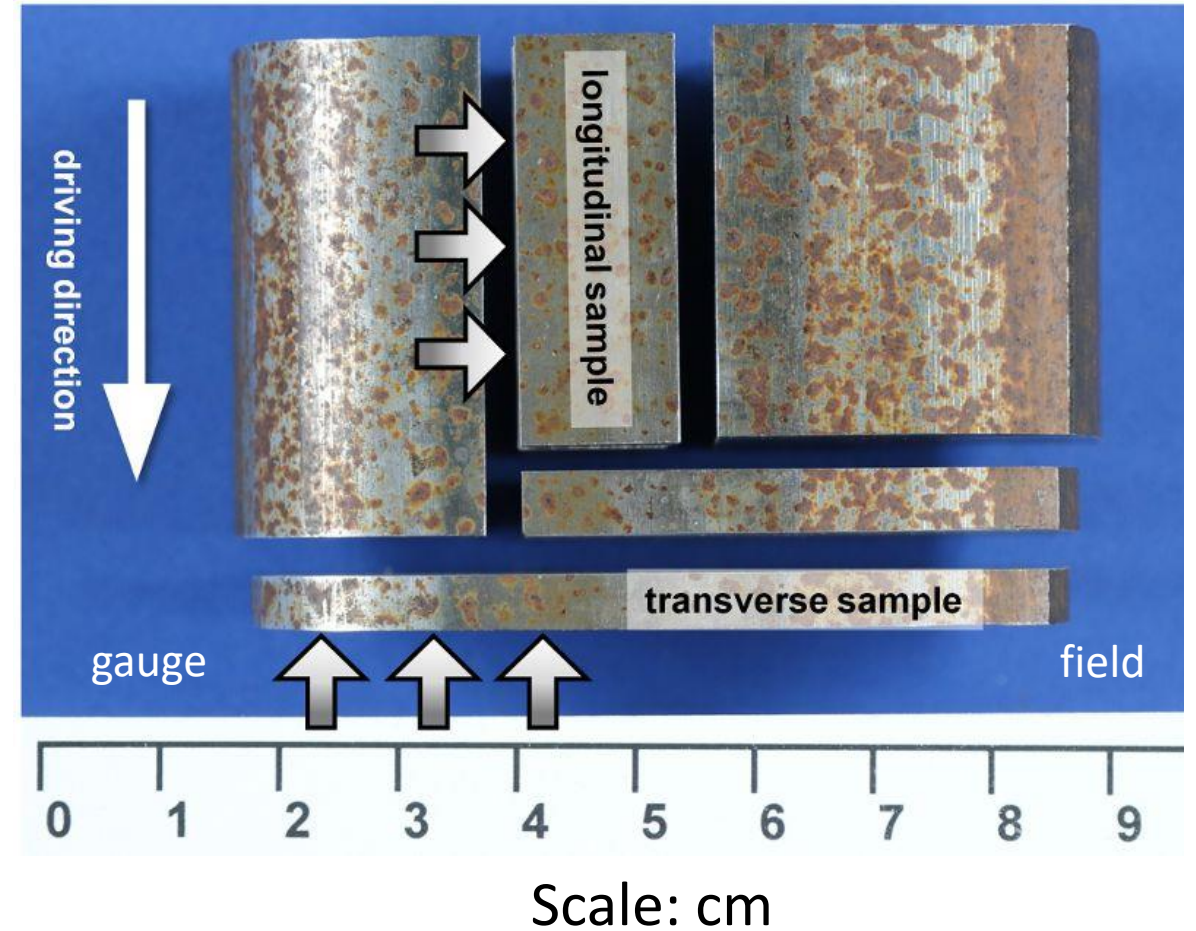
- Heat of the grinding process:
 - $T > 723^\circ\text{C}$ – austenite transformation
 - Significantly higher heat input over longer time for grinding
 - Grinding will lead to the formation of WEL

Z.Y. Zhang et. al., Thermal model and temperature field in rail grinding process based on a moving heat source, Applied Thermal Engineering 106 (2016) 855-864.

- Milling tests at the factory of LINSINGER and at a European IM
- EC tests before and after milling to characterise damage condition
- Metallographic analysis of rail samples:
 - Right after milling
 - A specific time / MGT traffic after milling



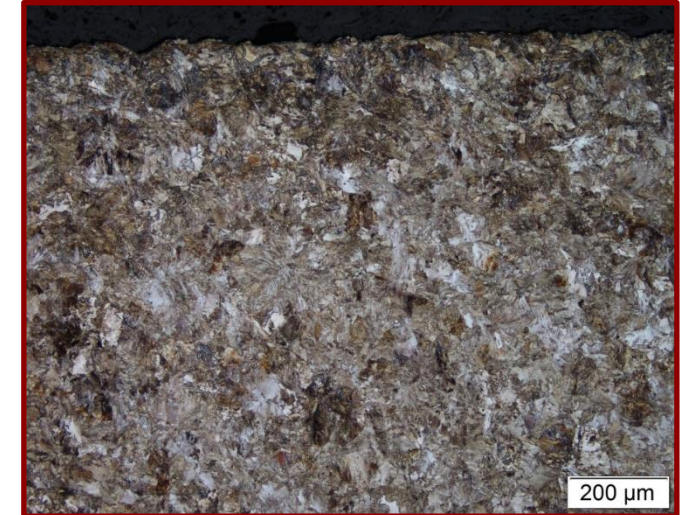
- Metallographic sectioning:
 - Longitudinal direction
 - Transversal direction
- Arrows indicate viewing direction



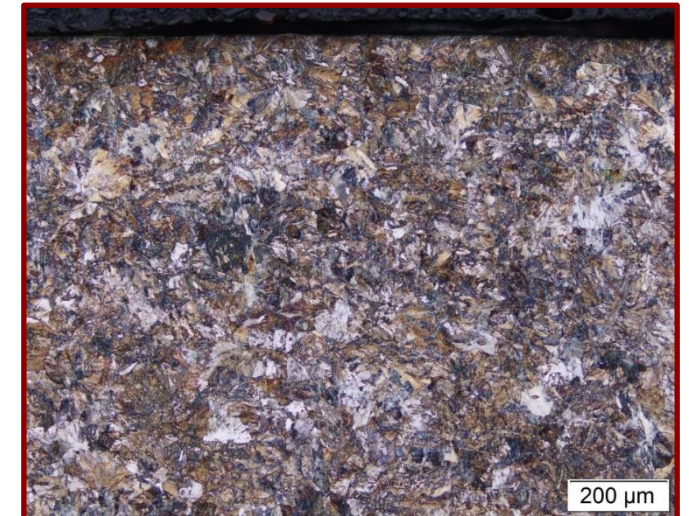
- Original conditions:
 - Rail grade R260
 - EC indicated 0.5mm max. crack before milling
 - 1 milling pass with 0.9mm metal removal
 - EC indicated no remaining damage after milling
- Rail sample removed from track directly after milling
- Micrographs revealed
 - Damage completely removed
 - No evidence of thermal material transformation
 - Smooth rail surface (no grinding marks)

condition 1

transverse



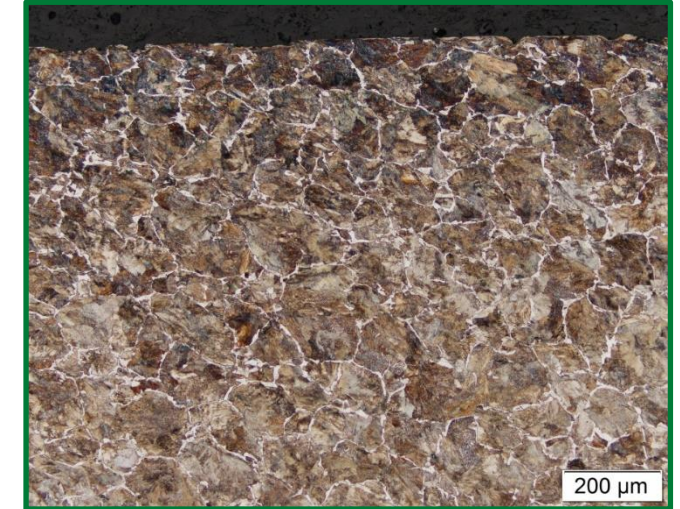
longitudinal



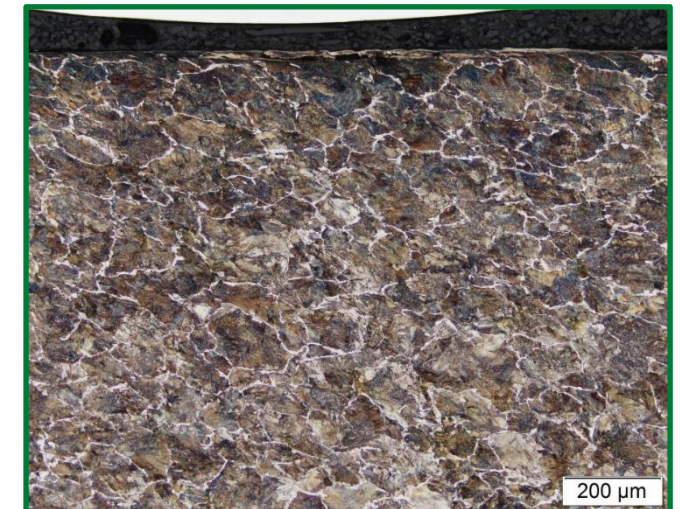
- Original conditions:
 - Rail grade R220
 - EC indicated 1.5mm crack depth
 - 2mm metal removal
 - Test area free of cracks after milling
- 11 days of traffic after milling – 0.12 MGT
- Micrographs revealed
 - Damage completely removed
 - No evidence of thermal material transformations
 - Smooth rail surface

condition 2

transverse



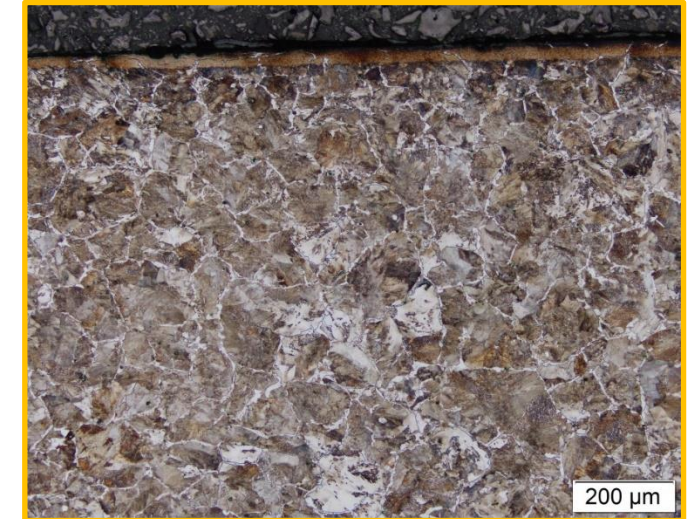
longitudinal



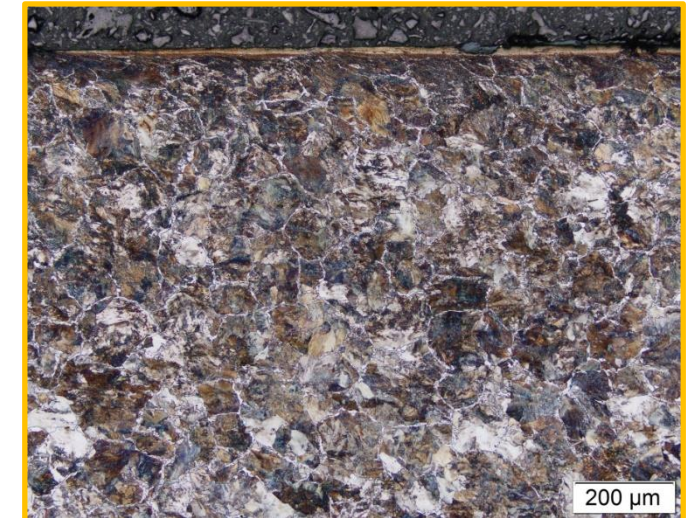
- Same location as sample before (condition 2) with same history
- 7 months of light traffic – 2.3 MGT
- Micrographs revealed
 - No cracks
 - Smooth rail surface
- WELs visible
 - Caused by train operations (traction)
 - Thickness around 30µm

condition 3

transverse



longitudinal

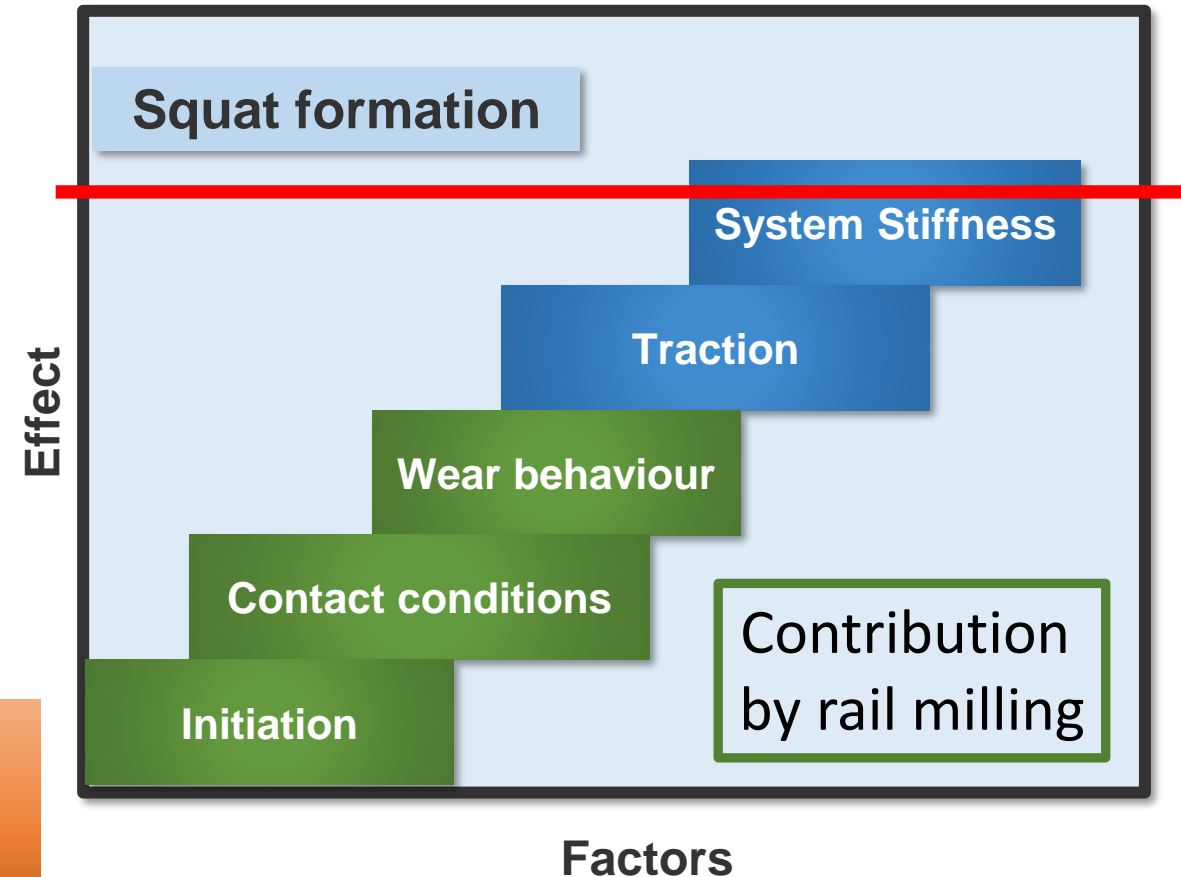


- DB specification: Milling for defects deep $> 0.8\text{mm}$
- Severe Squat defects
 - Measured depths up to 7mm
- High performance milling machine MG 31
- Regenerative Maintenance:
 - Complete damage removal
 - Max. 2 passes



- Contribution of rail milling to Squat mitigation:
 - Complete damage removal
 - Precise profile adjustment
 - Gentle surface treatment – no (new) initiation points
- Indicated by simulation results and track tests

**Squat solution only possible
on a system-level!**





THANK YOU FOR YOUR ATTENTION



Questions?

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