

Wheel squeal and flanging noise

Challenges in validation of friction management in the field and laboratory

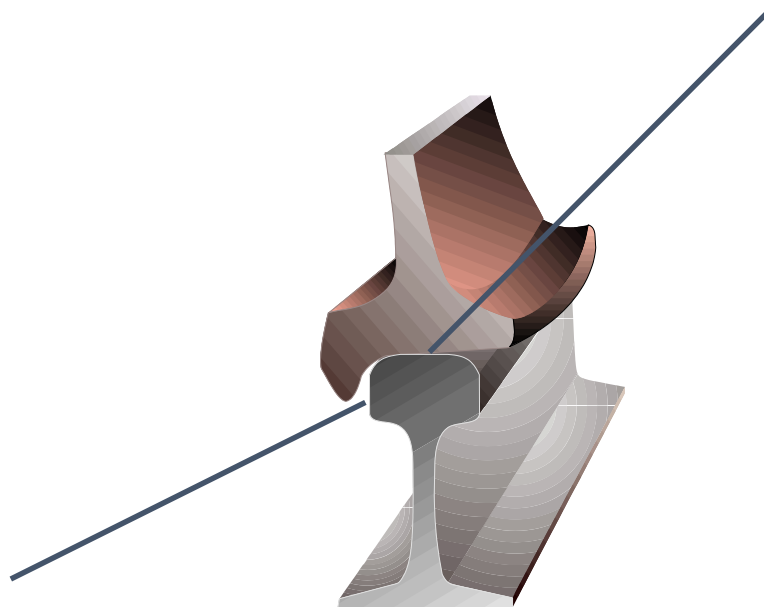
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30th June 2020

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- > Wheel squeal field trials
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Friction Management – Guiding Principles



- > **Gauge Face (GF) / Wheel Flange lubrication**

TARGET: COF < 0.15

- > Impacts:

- Rail / Wheel Wear
- Gauge Corner Cracking
- Flange Noise
- Derailment Potential (Wheel Climb)

- > **Top of Rail (TOR) / Wheel Tread Friction Modifier**

TARGET: COF ~ 0.35

- > Typical dry 0.6

- > Impacts:

- Rail / Wheel Wear
- RCF Development
- Top of Rail Noise
- Corrugations

- > Reduced lateral forces

- > Switch protection

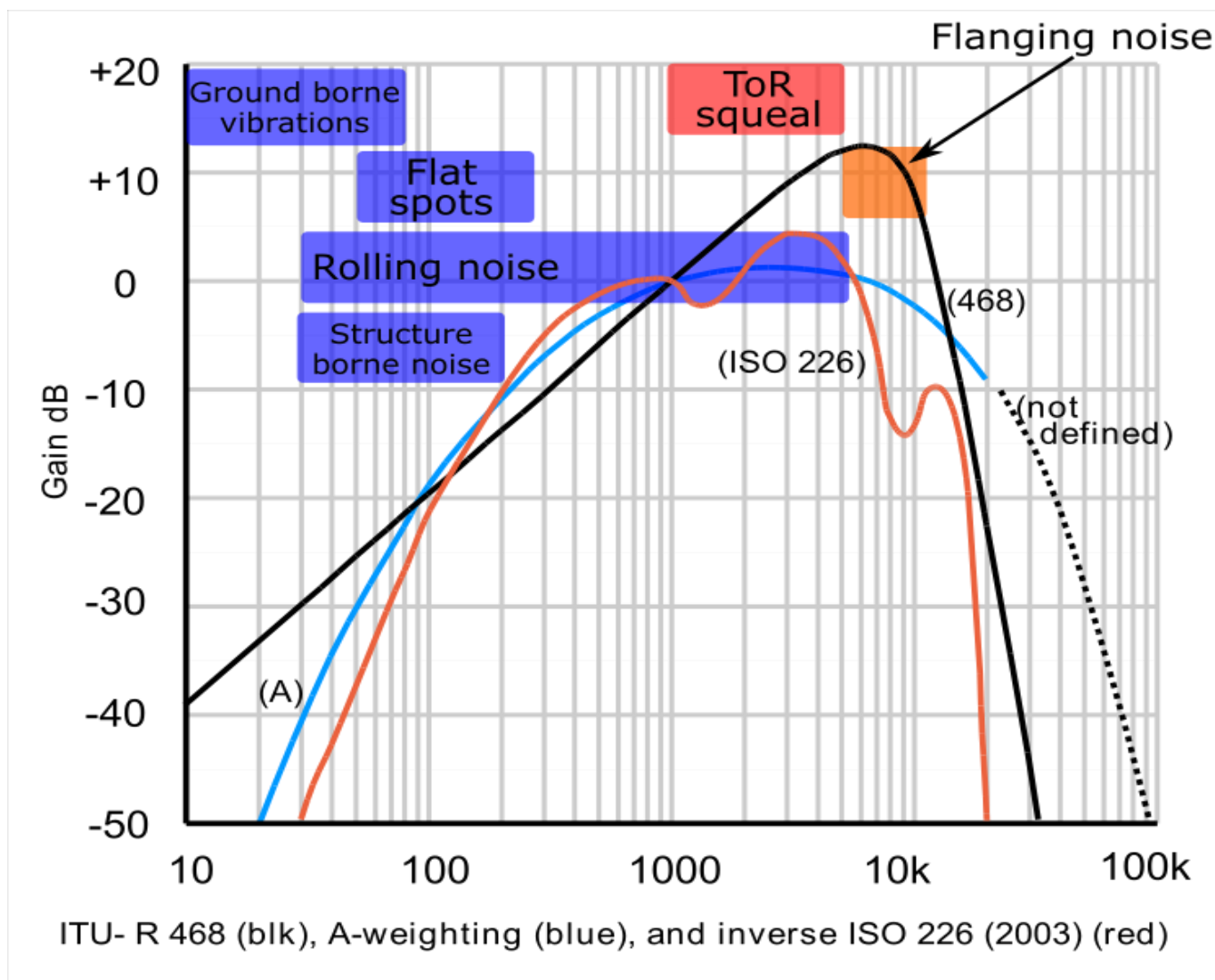
- > Reduced traction energy consumption

Background to rail wheel noise

Noise: Spectral ranges

Noise Type	Frequency range [Hz]
Rolling	30 – 2500
Rumble (including corrugations)	200 – 1000
Flat spots	50 – 250 (speed dependant)
Ground Borne Vibrations	30 – 200
Top of rail squeal	1000 – 5000
Flanging noise	5000 – 10000

Human perception of noise



Squeal and Flanging Noise

Top of rail wheel squeal noise



- High pitched, tonal squeal (predominantly 1000 – 5000 Hz)
- Prevalent noise mechanism in “problem” curves, usually < 300m radius
- Related to both **negative friction** characteristics of Third Body at tread / top of rail interface and **absolute friction** level
 - Stick-slip oscillations
 - Leading wheelset, inside wheel

Flanging noise



- Typically a “buzzing” OR “hissing” sound, characterized by broadband high frequency components (>5000 Hz)
- Affected by:
 - Lateral forces: related to **friction on the top of the low rail**
 - Flanging forces: related to friction on **top of low and high rails**
 - Friction at the flange / gauge face interface

Corrugation noise



Noise due to corrugation with occasional wheel squeal and flanging noise

Corrugation noise

- **Low pitched rumbling noise due to the presence of corrugation on the running band of the rail**

Field trials

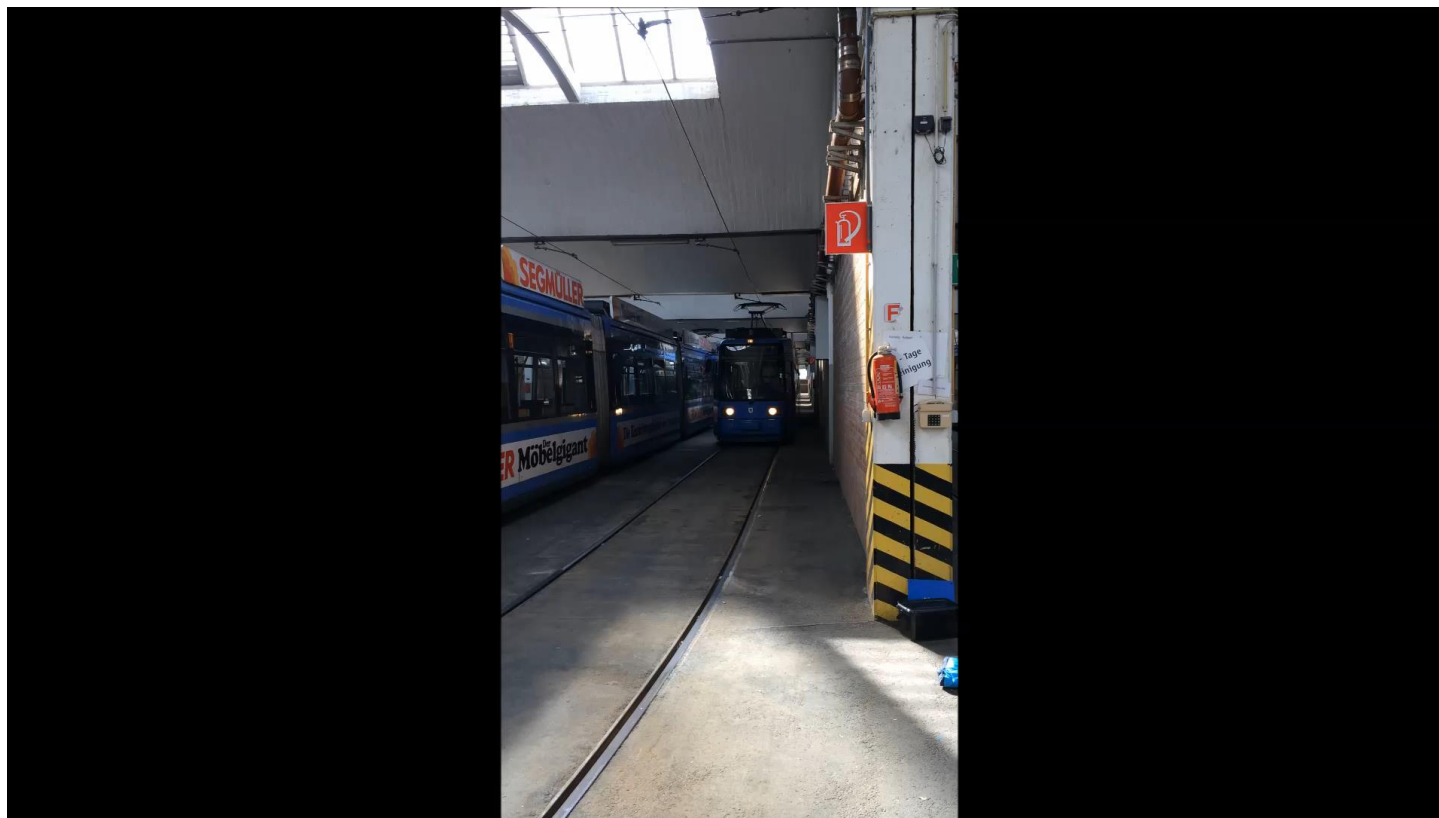
FM Focus: Noise/Corrugation

Baseline – No TOR FM application



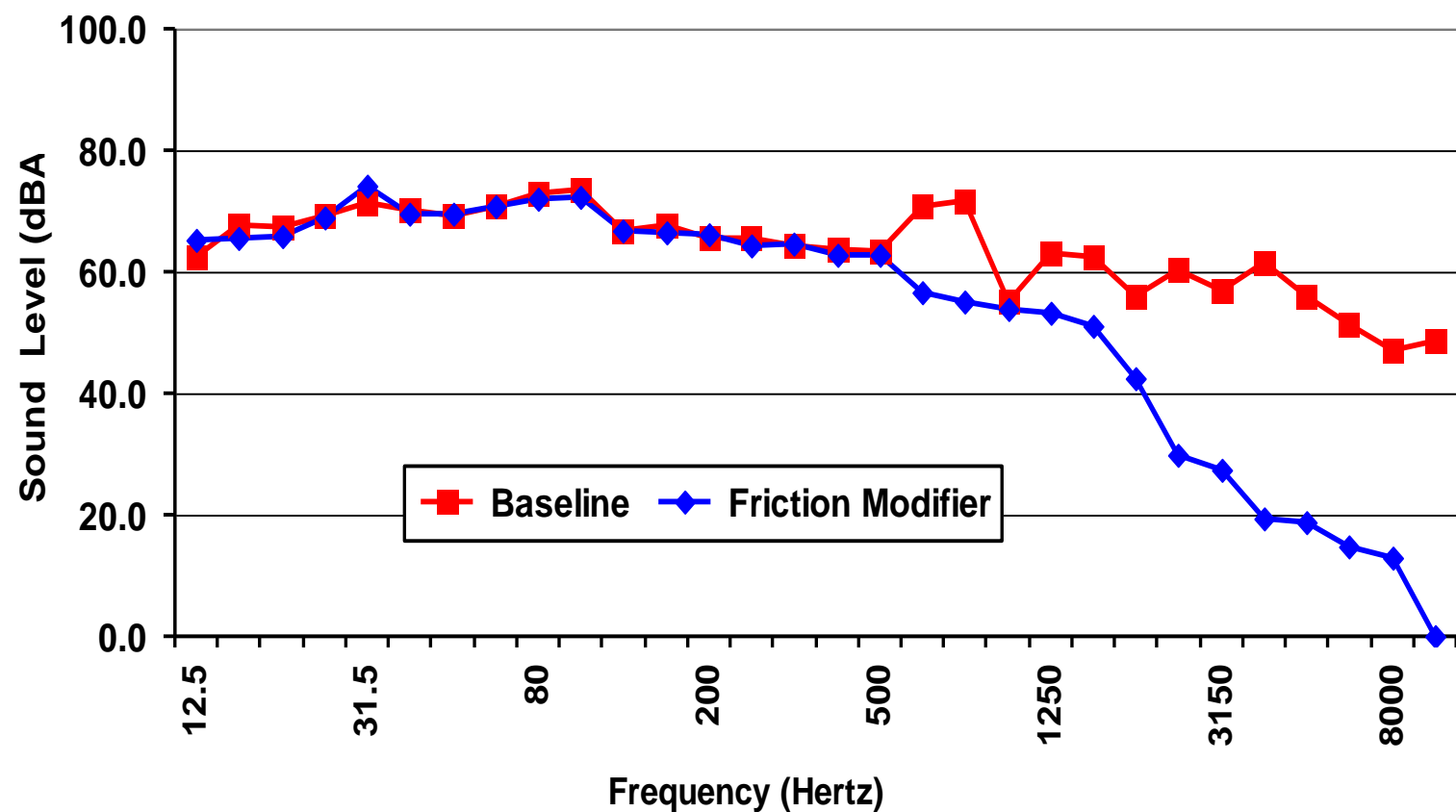
FM Focus: Noise/Corrugation

AFTER TOR FM application - manual



Spectral sound distribution: Trams

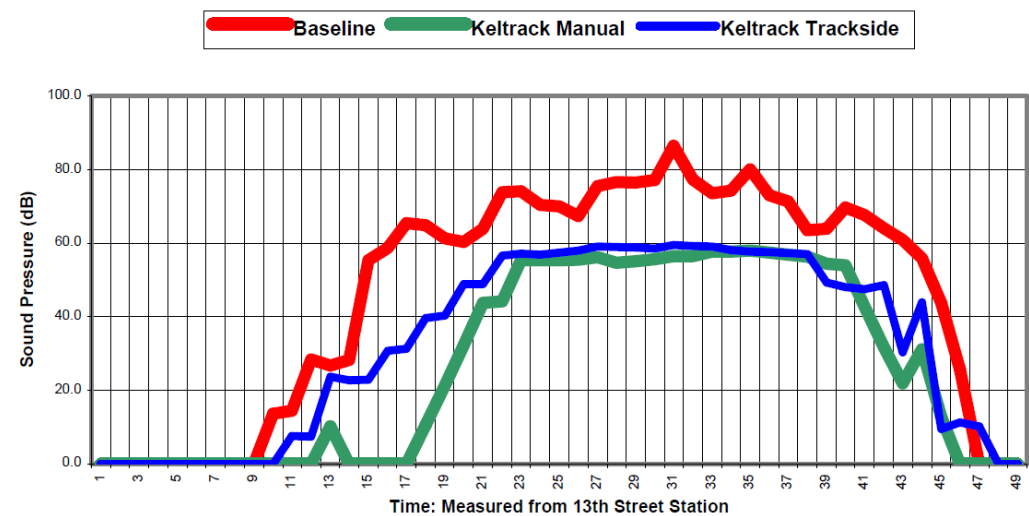
> Effects of frictional conditions



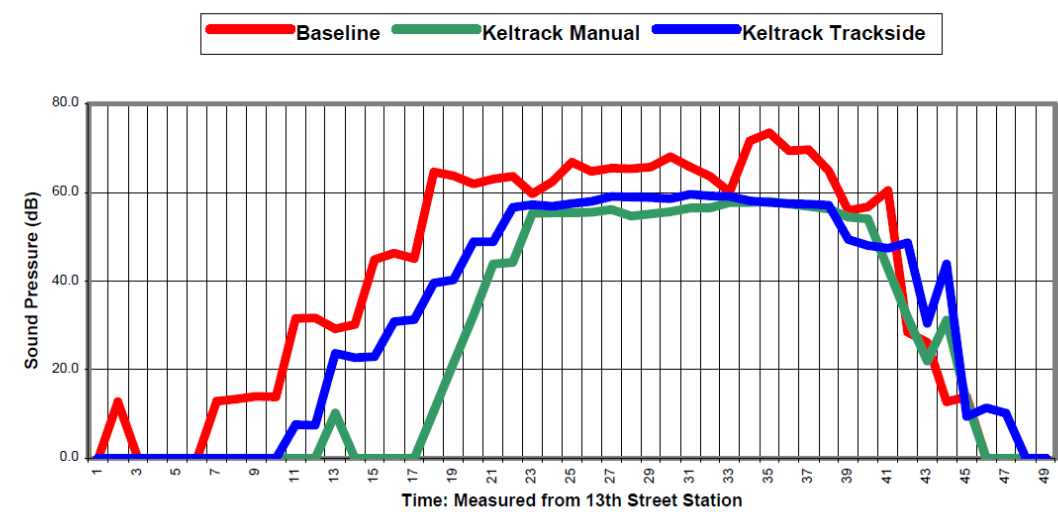
Spectral sound distribution: Trams

> Effects of frictional conditions

Average Sound Pressure versus time at 1.6 kHz



Average Sound Pressure vs. Time at 2.5 KHz



Field trials

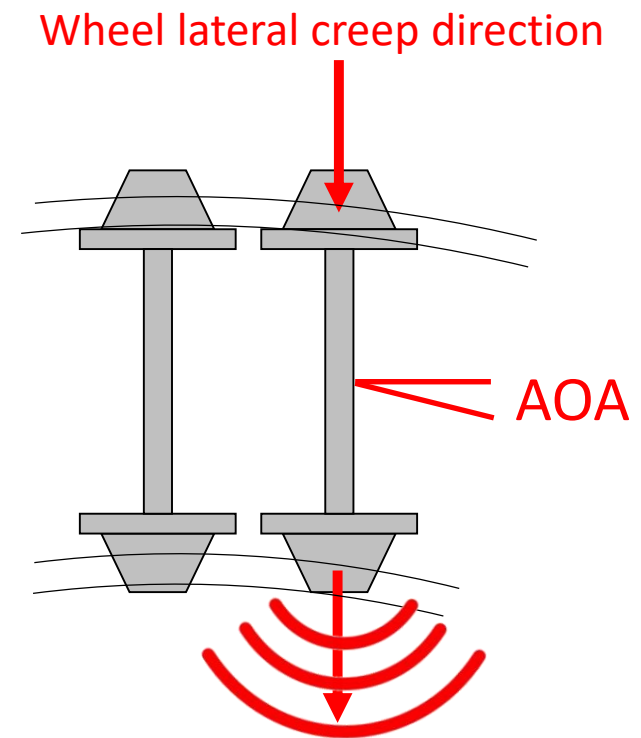
- > Typical field trials compare baseline measurement to application of top of rail materials
- > Noise can be very specific to:
 - Vehicle
 - Bogie steering – primary yaw stiffness
 - Wheel profile
 - Location – curve/cant
 - Running speed
 - Weather
 - Rain and moisture (morning dew) particularly large impacts
 - Humidity
 - Rail and wheel contamination
 - Measurement location (reflections)
- > Don't necessarily get squeal from every bogie

Wheel squeal – conventional theory

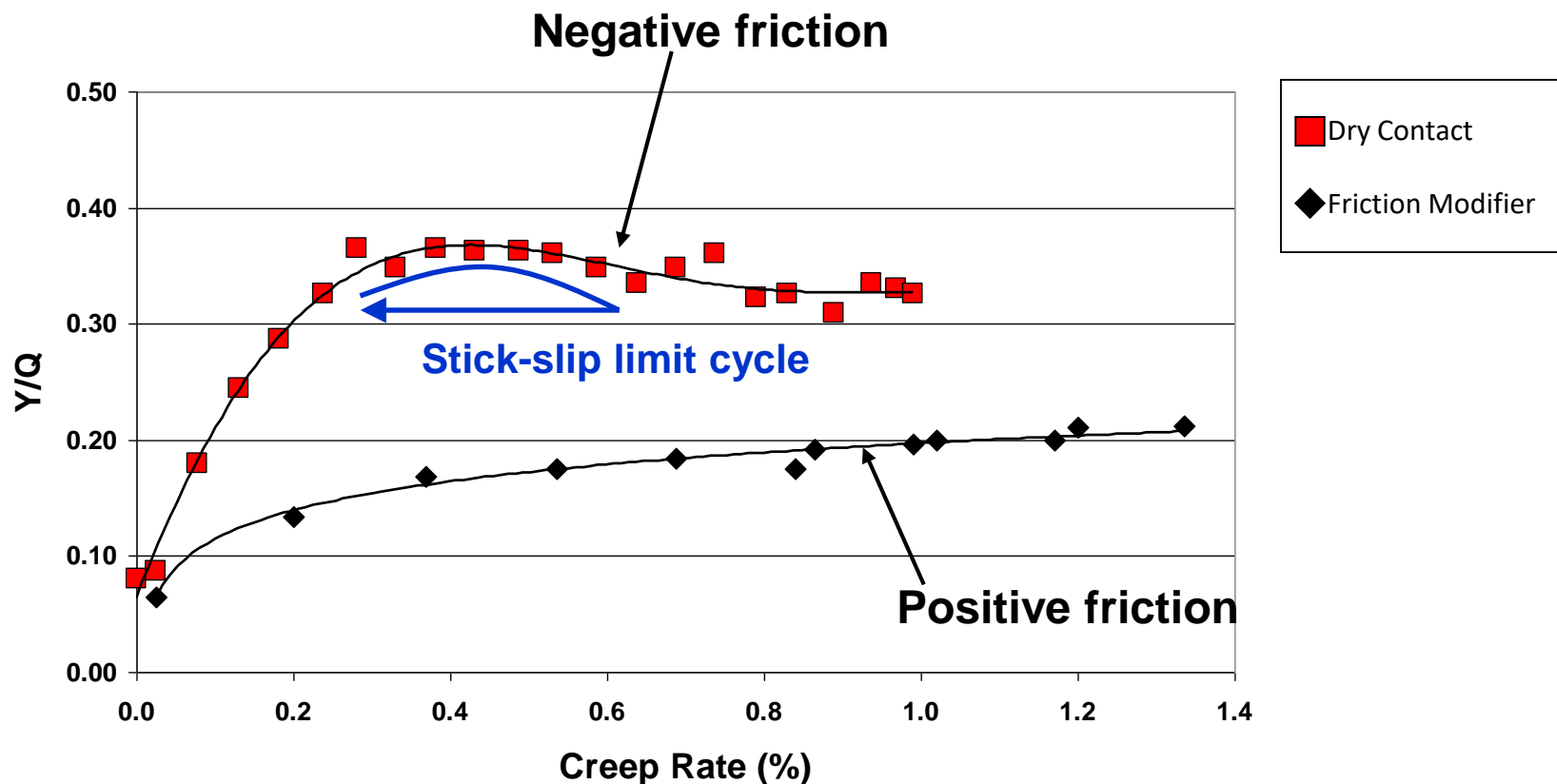
Lateral creepage of the wheel -
prime cause of squeal

- Particularly for the leading inner wheel of a bogie
- stick-slip mechanism of this creep force

Rudd 1976, Remington 1985

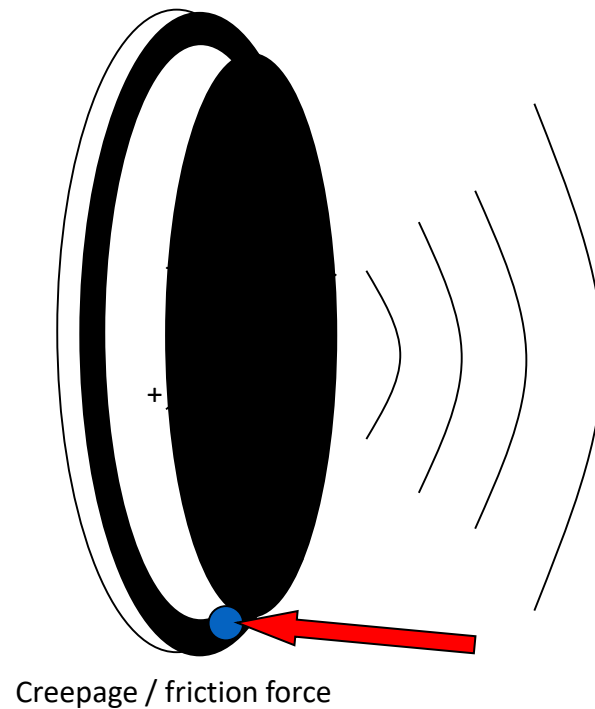


Absolute Friction Levels and Positive/Negative Friction – conventional theory



* Replotted from: “Matsumoto a, Sato Y, Ono H, Wang Y, Yamamoto Y, Tanimoto M & Oka Y, Creep force characteristics between rail and wheel on scaled model, *Wear*, Vol 253, Issues 1-2, July 2002, pp 199-203.

Absolute Friction Levels and Positive/Negative Friction – conventional theory



Frequency response of
the wheel

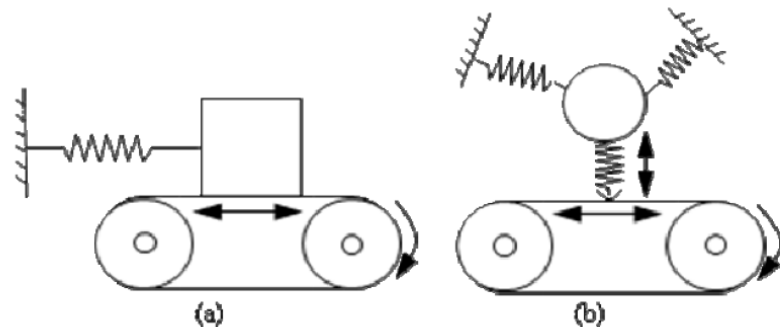
Alternative theory

Mode Coupling Instability Mechanism

- > Jiang, Anderson and Dwight, 2015
- > Further analysis by Bo Ding 2018

Theory:

- > Based on commonly accepted theory for squeal in braking systems. A coupling of vibration in two different directions
- > Wheel/rail interface subject to vertical and lateral vibrations and forces



Alternative theory

Mode Coupling Instability Mechanism

- > The lateral frictional force between the wheel and the rail is related to the normal (vertical) force, so a natural coupling
- > $F = \mu N$
- > If wheel vertical and lateral vibration frequency modes are close
- > Then friction coefficient increases to a critical threshold,
 - > vertical and lateral oscillations become out-of-phase
 - > friction force, which depends on the vertical force, is therefore out-of-phase with the lateral motion => unstable positive feedback.

Alternative theory

> Mode coupling instability mechanism

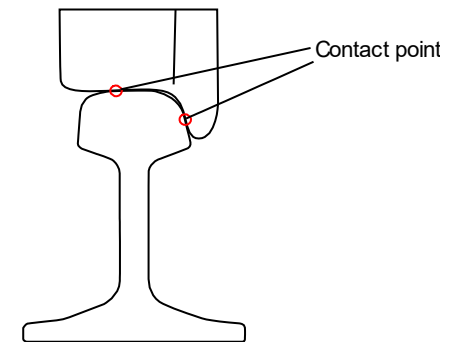
> Curley, Anderson, Jiang and Hanson – track study

- Found noise from wheels on inner and outer rail
- Running bands in different locations on gauge corner of inner and outer rail
- Track form had an influence
- Found TOR FM had benefit when applied to both rails, but in some cases when applied to inner rail only no benefit
- Counter to normal theory gauge corner lubrication also had a benefit for wheel squeal

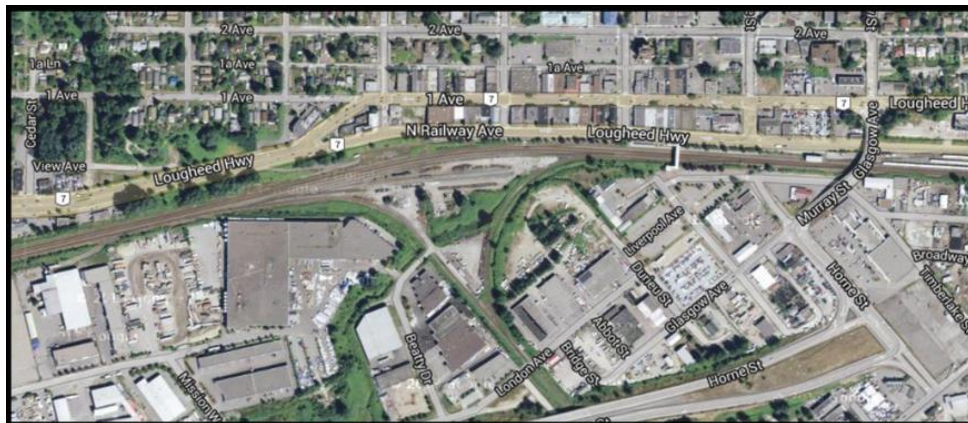
Alternative theory

> Mode coupling instability mechanism

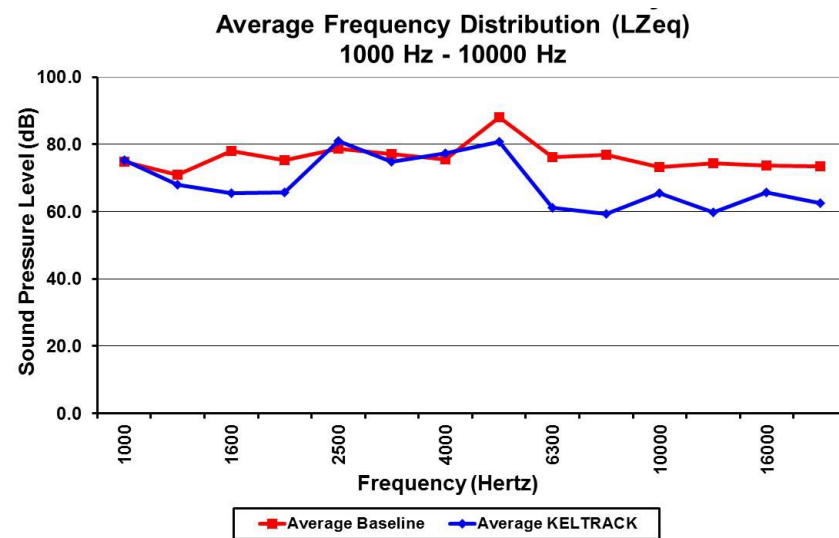
- > For all these theories friction between the wheel and the rail still key.
- > Work carried out by Bo Ding 2018 – studied slip/stick mechanism, mode coupling instability, and third potential mechanism wheel rail coupling
- > 2 point contact – not studied much wrt wheel squeal



Freight trial with two types of water based TOR FMs



- > Two versions of top of rail friction modifiers tested
 - Both products have high positive friction characteristics
 - Similar intermediate friction
 - Different binders and tackiness
 - One product retained more on wheel (less effective), other transferred more to rail
 - One product much more effective than the other in noise reduction
- > Oil and grease based top of rail materials – difficult to balance noise reduction with braking and traction performance
- > Difficult to predict noise performance from laboratory testing

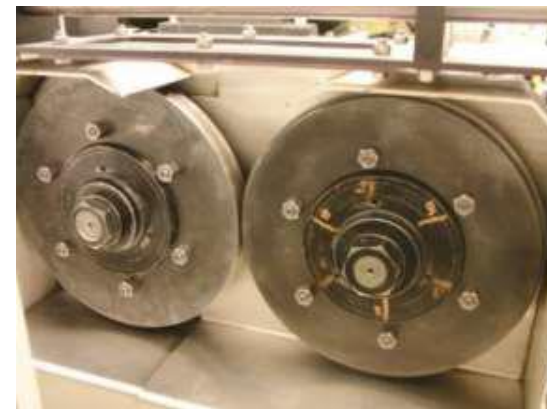


Laboratory investigations into wheel squeal

Laboratory testing

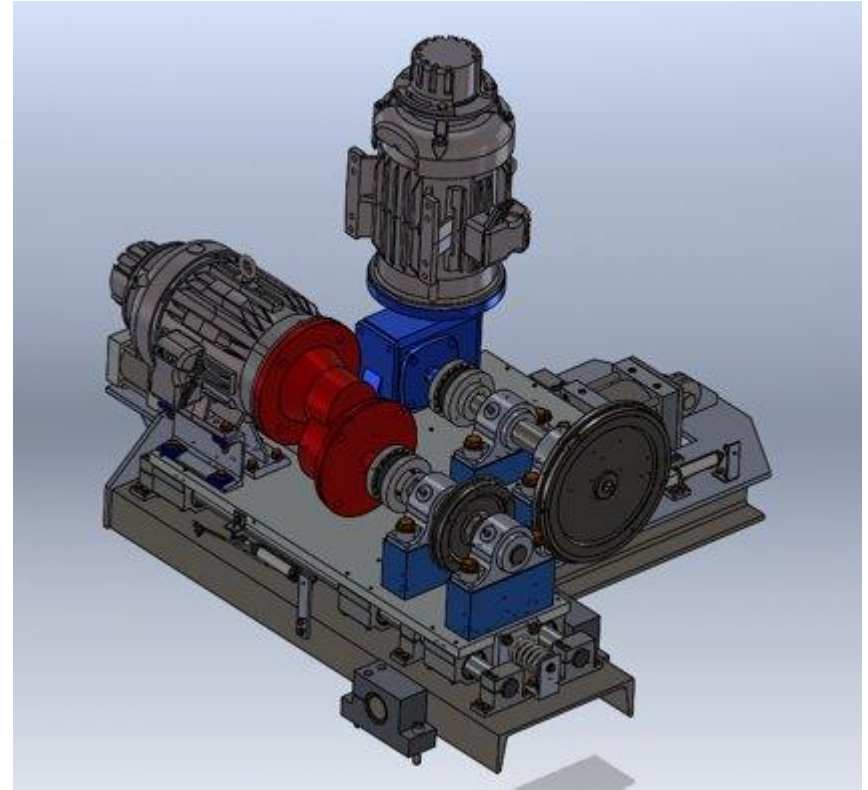
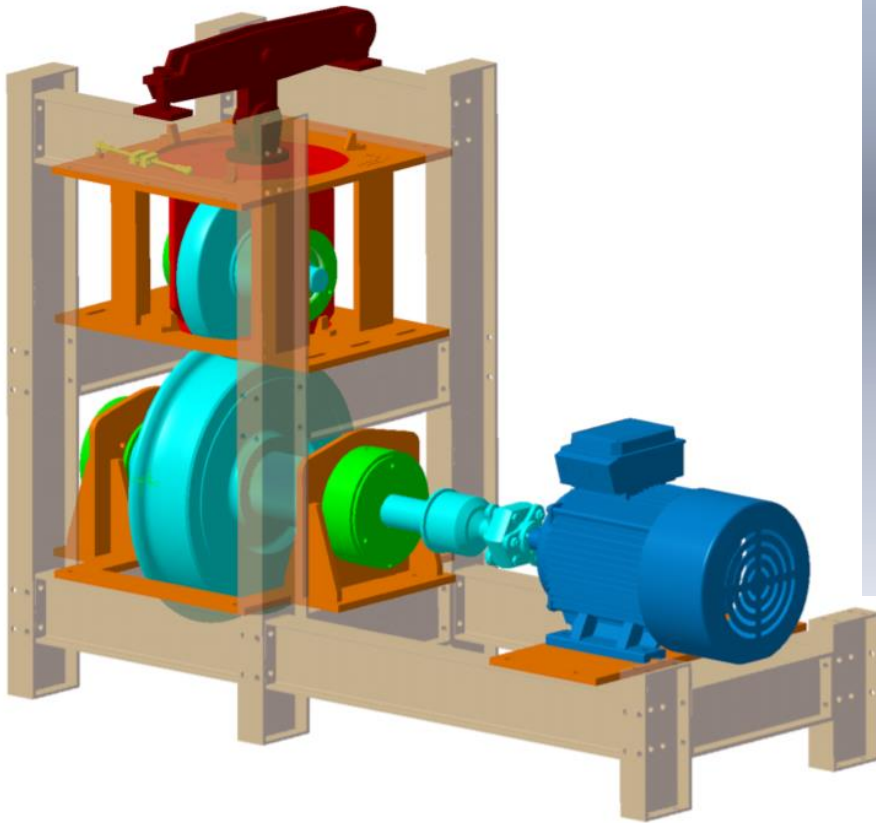
> Twin disc type testing

Eg. TNO test rig



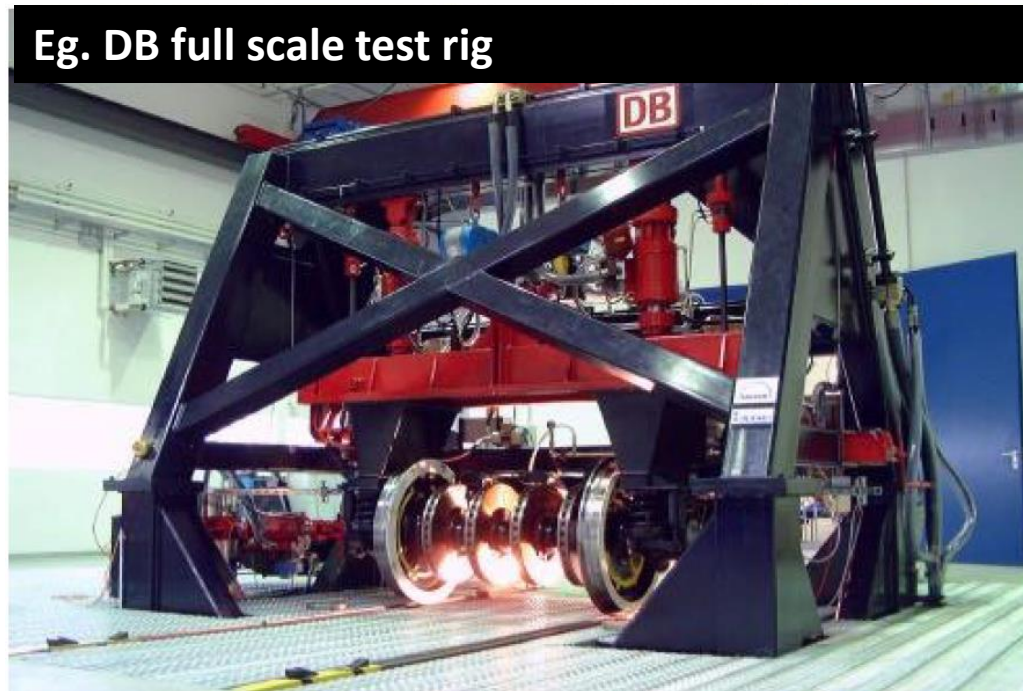
Laboratory testing

> Scaled rigs



Laboratory testing

- > Full scale test rigs



UIC study 2005

- > Compared results wheel squeal mitigation of different products on laboratory test rigs and on site measurements
 - Issue of application rate, too

		TOR FM1 (water based)	TOR FM2 (oil based)	TOR FM3 (oil based)	TOR FM4 (oil based)	Water
Lab	TNO rig	Y	Y	Y	Y	
	DB rig	Y	Y			Y
Field	Site 1	Y	N	N	N	
	Site 2	N				
	Site 3	Y				Y

**Comparison of wheel squeal for different FMs in lab and in the field –
(Y – Noise reduced, N – no significant noise reduction)**

Wheel squeal mitigation

- > Good understanding of effective mitigation methods
 - Top of rail/tread friction modifiers (lubrication) – all theories point to the importance of friction control
 - Bogie/wagon design
 - Distance between axles
 - Vehicle steering – primary yaw stiffness
 - Wheel dampeners
 - Wheel and rail profile
 - Track form dynamics

Challenges

Product development

- > Need on track trials and case studies to prove noise reducing properties.
- > Lab scale test can give an indication – but not the whole story
 - Slows down product development – need to produce larger batches
 - Some products are easier to test by manual application than others
 - Eg on board - solid stick friction modifiers and lubricator sticks
 - to test in the field do you swap out the sticks from the whole fleet to negate the effect of other sticks on the performance? – In a smaller limited trial do you build up sufficient film thickness
- > Need for better lab scale noise testing
- > Understanding of required film thickness/application rate

End customer

- > Needs case studies and evidence of on track performance
- > Cannot rely on lab tests and friction data alone
- > Squeal/noise remains a major issue for most railways/metros

“curve squeal remains one of the least understood railway noise sources despite the continuing efforts over recent decades” Jiang, Anderson and Dwight, 2015

Questions