

Experimental study on wear and RCF damage of wheel/rail materials under complex environment conditions

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- 1. Wear and RCF of wheel/rail under complex environment
 - Low temperature
 - Windblown sand condition
- 2. Microstructure evolution of wheel/rail materials
- 3. Wear and RCF prediction
 - Wear rate-Tγ/A
 - Shakedwon map
- 4. Rail grinding



Low temperature



High speed train wheel







2013.7.8

RCF damage is severer in winter



1.1 Effect of temperature: Experimental equipment

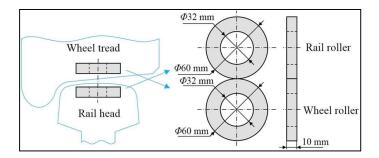
- ❖ Wheel/rail twin-disc rigs
- ❖ Low temperature (0~-60°C)

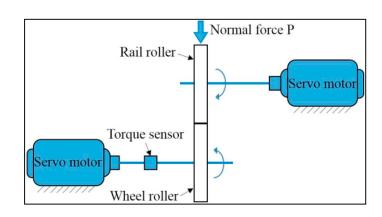


JD-1 wheel/rail simulation rig



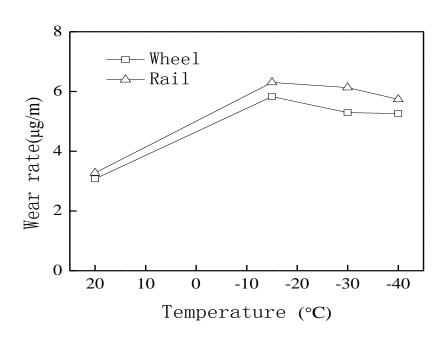
Twin-disc rig with temperature control system







Wear



- ❖ At low temperature: wear ↗ ↗
- **❖** Low T from -15°C to -40°C : wear ∨



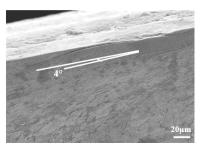
RCF

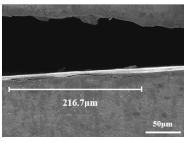
20°C

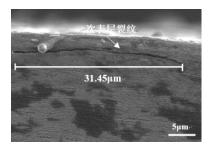
-15°C

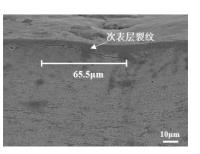
-30°C

-40°C









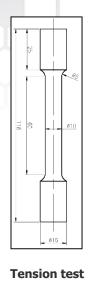
*	At low temperature: RCF / /
*	Low T
*	Wear & R silver trend

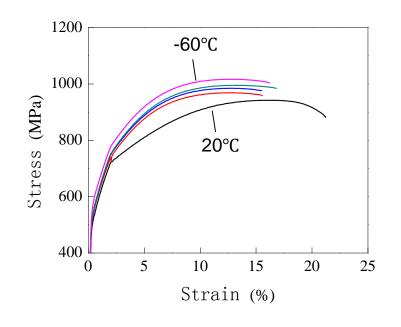
Tamananatama	Surface cracks		
Temperature	Angle (°)	Depth (µm)	
20 °C	8.14±2.11	11.76±2.21	
-15 ℃	14.28±8.38	12.06±10.41	
-30 °C	10.66±5.59	6.20±2.17	
-40 ℃	9.33±3.77	7.68±2.76	

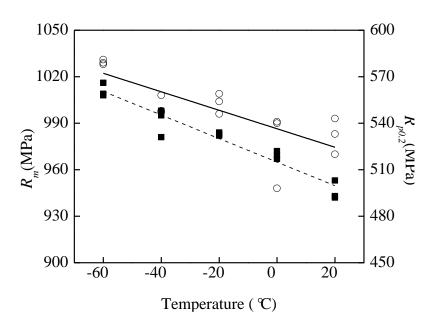
Temperature _i	Subsurface cracks	
remperature	Length (µm)	
20 °C	38.77±2.89	
-15 ℃	74 .97±51.33	
-30 ℃	57 .76 ± 46.84	
-40 °C	52 .69±39.14	



Mechanical properties





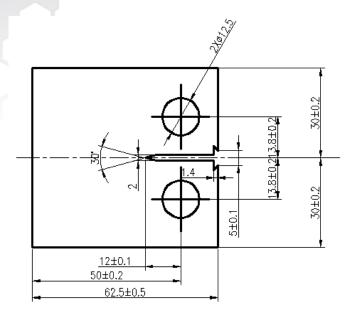


Temperature >:

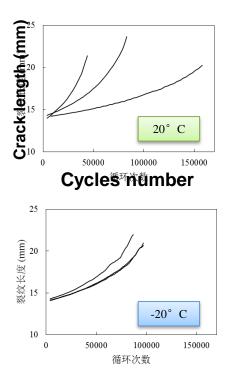
- ❖ Ultimate tensile strength R_m ↗
- ❖ Yield strength R_{p0.2}

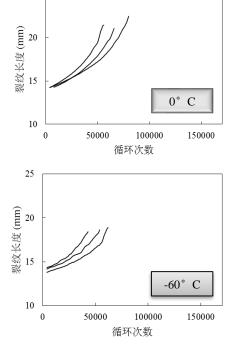


Mechanical properties



Repeated tension and compression test

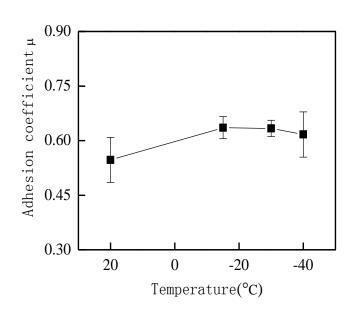


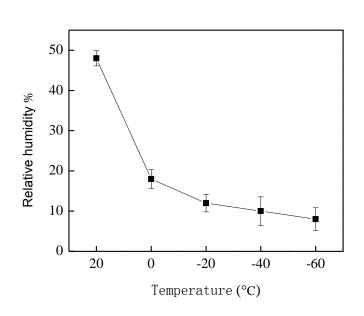


Temperature >: Crack growth rate ↗

Rolling sliding contact

Adhesion coefficient





- At low temperature: RH↘↘, CoA ↗ ↗, Tangential force ↗ ↗
- Low T from -15°C to -40°C : RH>, CoA >, Tangential force >



Room T **>** low T:

- ❖ Strength ↗
- ❖ Crack growth rate ↗ (brittleness ↗)
- ❖ Wear / /
- ❖ RCF / /

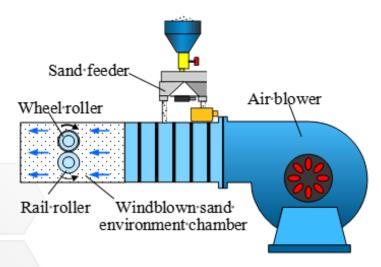
low T -15°C > -40°C:

- ❖ CoA
 ↘
- ❖ Wear >
- ❖ RCF
 ↘





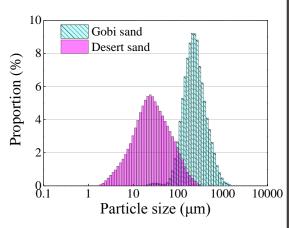
Windblown sand environment



Twin-disc rig with windblown sand

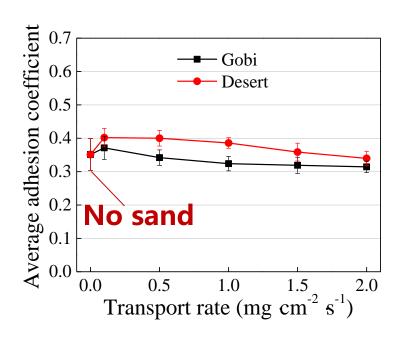








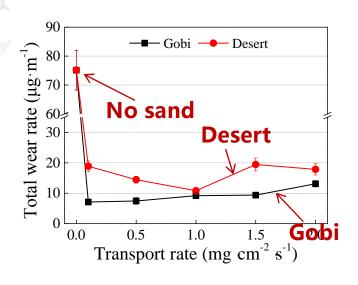
Adhesion coefficient

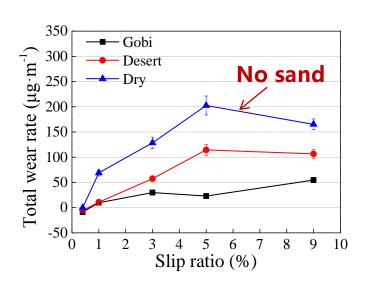


- ❖ Feed rate / : CoA \(\sigma\)
- ❖ Gobi < desert</p>



Wear

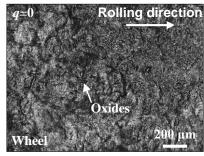




Gobi < desert < no sand



RCF Wheel



No sand

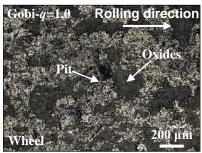
Feed rate=0.1

Gobi-q=0.1 Rolling direction

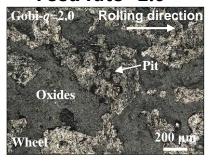
Oxides

Wheel $200 \, \mu m$

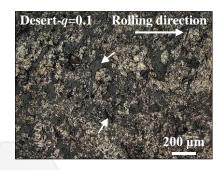
Feed rate=1.0

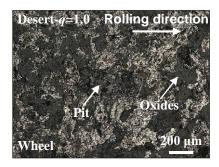


Feed rate=2.0



Gobi





Desert-q=2.0 Rolling direction

Pit
Oxides

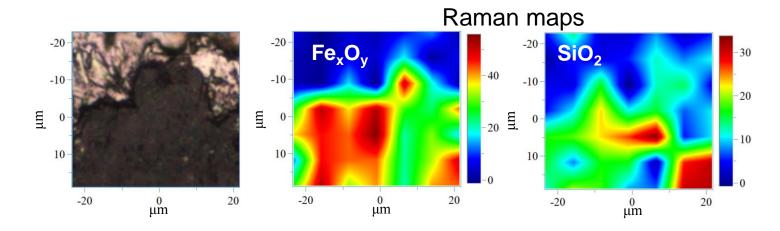
Wheel 200 μm

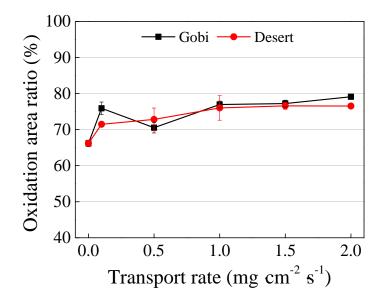
Oxides





RCF Wheel





Oxides content /



RCF Rail



No sand

Feed rate=0.1

Gobi-q=0.1 Rolling direction

Surface crack

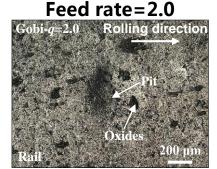
Rail 200 µm

Feed rate=1.0

Gobi-q=1.0 Rolling direction

Pit

Rail 200 µm

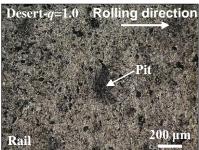


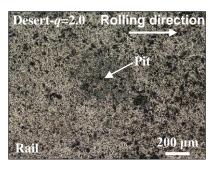
Surface damage

- No sand : dense RCF
- ❖ Gobi < desert</p>
- **❖** Feed rate **↗** : RCF **↘**

Gobi



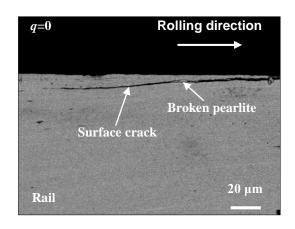




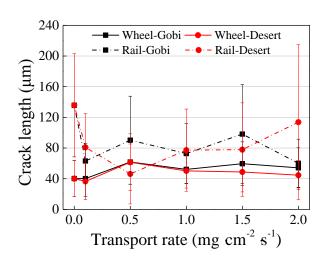
Desert

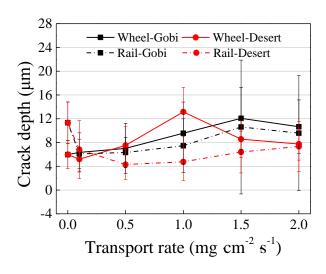


RCF Rail

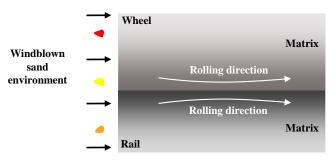


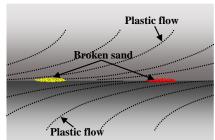
RCF observed on cross sections

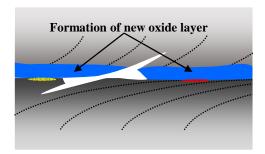


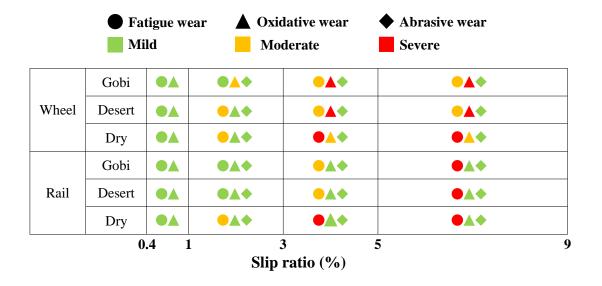










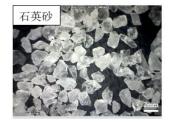


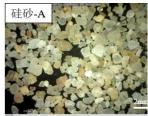


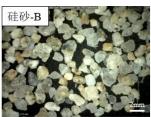
Windblown sand vs. Sanding



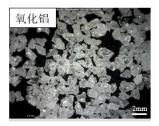
□ For sanding





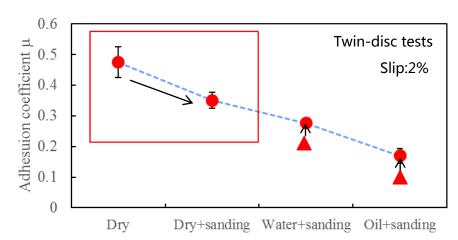






>1mm





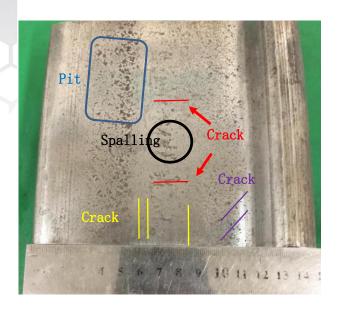


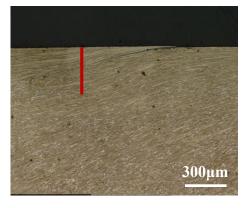
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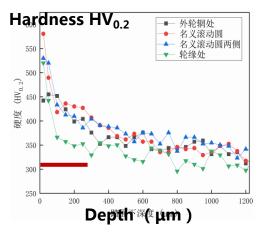


2. Microstructure evolution of wheel/rail materials

Locomotive wheel







Rail





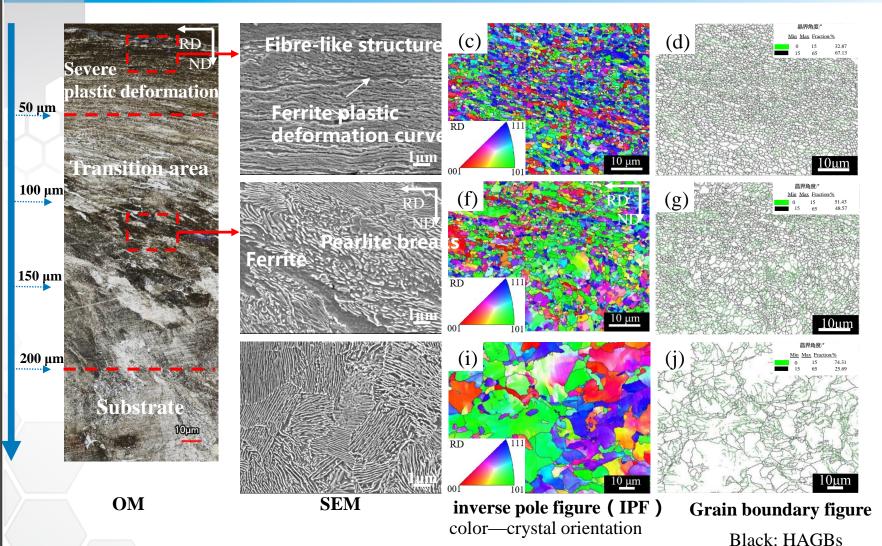




2. Microstructure evolution of wheel/rail materials

Wheel, 0.91%, 850MPa

Green: LAGBs

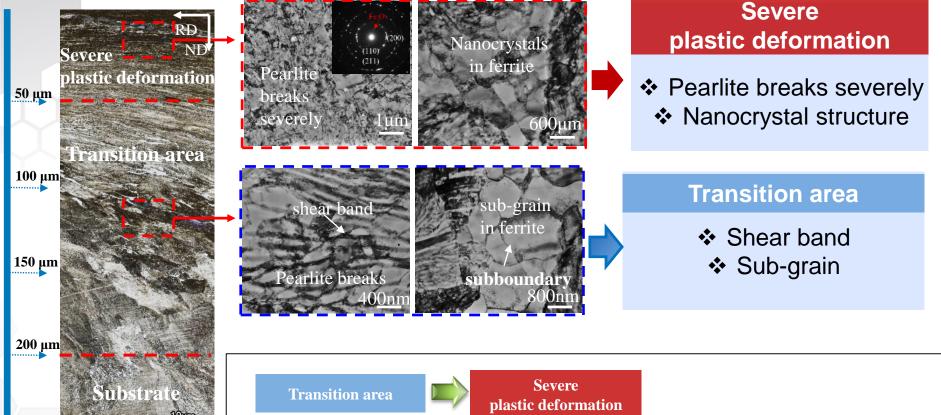


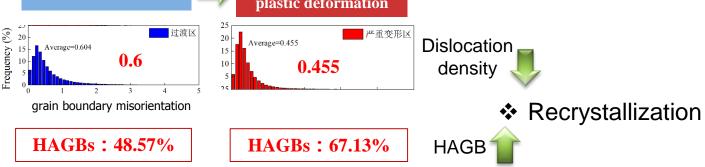
- ❖ Pearlite breaks ❖ Ferrite plastic deformation curve
 - ❖ Fibre-like structure ❖ Grain size decreases



2. Microstructure evolution of wheel/rail materials

Wheel, 0.91%, 850MPa



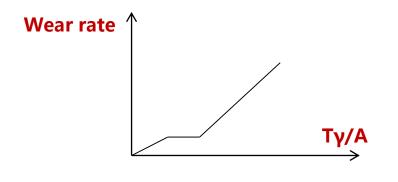




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Wear rate – Tγ/A model : basis of wear prediction



Wear rate : μg/m/mm²

T: tangential force

γ : slip ratio
A : contact area

Construction of Wear rate – Tγ/A model for individual mateiral



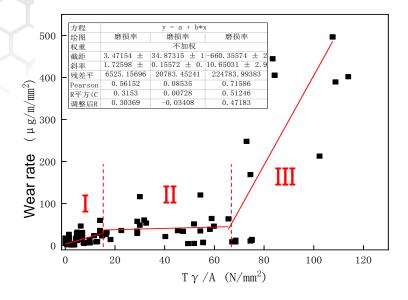
Twin-disc tests

Axle load Speed Slip ratio



3.1 Wear rate – Tγ/A model

U75V rail

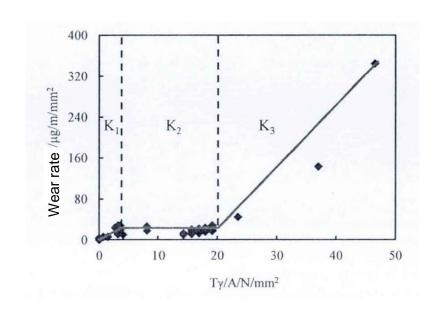


I region : y = 1.73x + 3.5

II region : y = 0.16x + 34.9

III region : y = 10.7x - 660

CL60 wheel



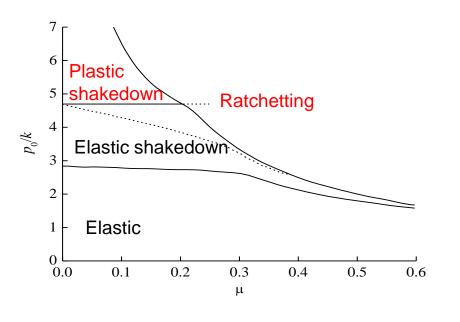
I region: y = 3.58x (x<5)

II region: y = 17.9 (5<x<20)

III region : y = 12.3x - 228 (20<x)



Shakedown map: basis of RCF prediction



p₀: maximum contact pressure

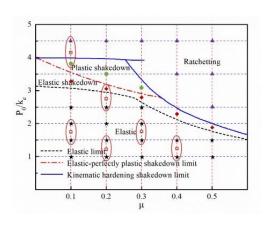
k: pure shear yield strength

μ: traction coefficient

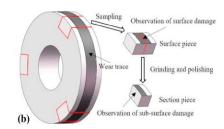
- Plastic shakedown region
- Ratchetting region



Construction of shakedown map for individual mateiral



- U75V rail
- Experimental details
- Different µ values: via different slip ratios
- Different P₀ values
- Analysis of samples



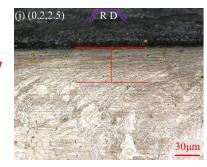
- Stable wear/damage state: 40 000 cycles
- Determination of damage types, i.e. shakedown map regions
 - Ratchetting region: RCF cracks
 - Plastic shakedown region: No cracks + plastic flow
 - Elastic shakedown region: No plastic flow
 - Elastic region



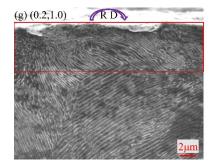
Ratchetting region: RCF cracks



Plastic shakedown region: No cracks + plastic flow



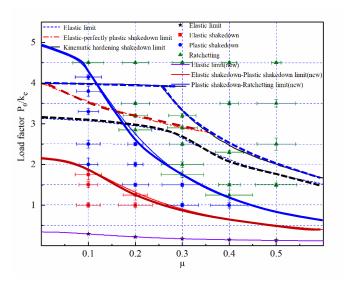
Elastic shakedown region: No plastic flow



Elastic region



❖ U75V rail



Boundaries were drawn according to the RCF damage



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RCF damage



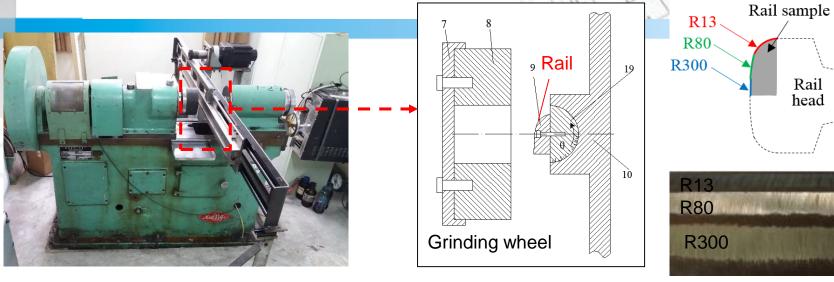
Profile change (wear)



Rail grinding



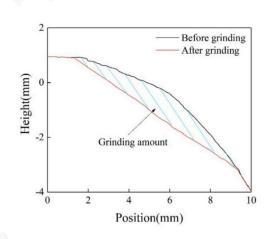


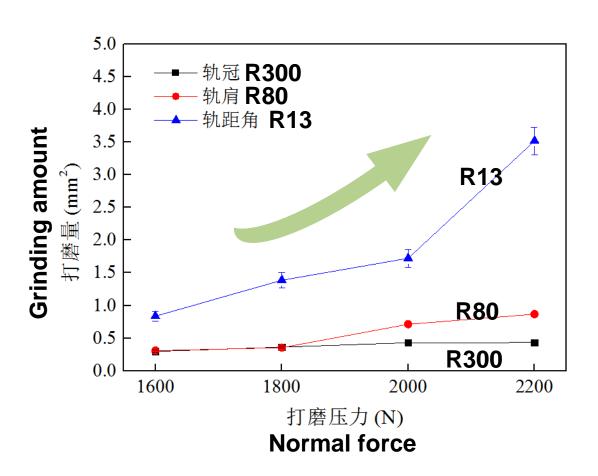


Position	Normal force	Forward speed (km/h)	Rotational speed of stone (r/min)
R13, R80, R300	1600, 1800, 2000, 2200	1, 2, 3, 4	2500, 3000, 3500, 4000

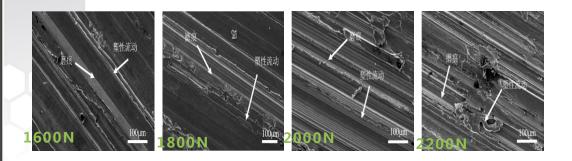
Analysis: surface mophology, burn, white etching layer, etc







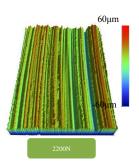




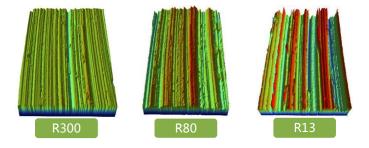


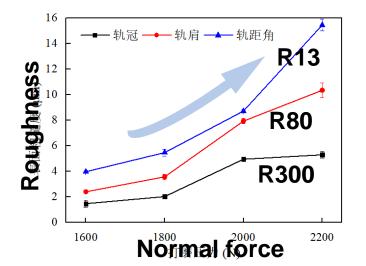




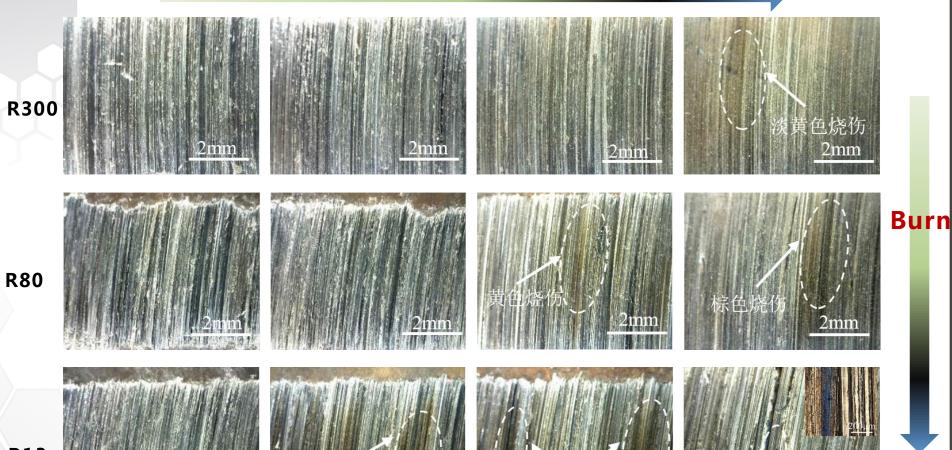


Normal force ₹, roughness ₹
Radius ₹, roughness ₹









R13



1800N



2200N



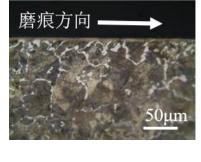


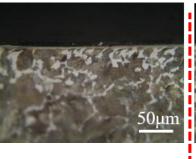
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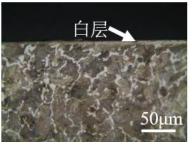
WEL

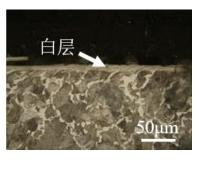


R300



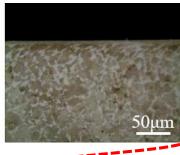


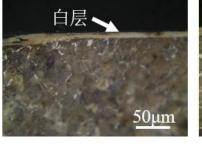


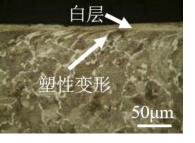


R80

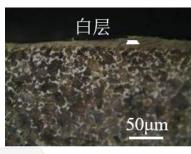


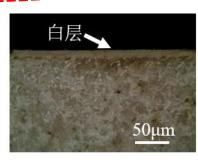


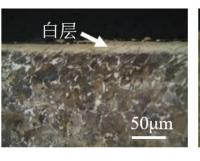


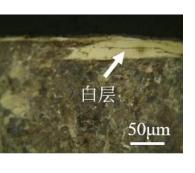


R13









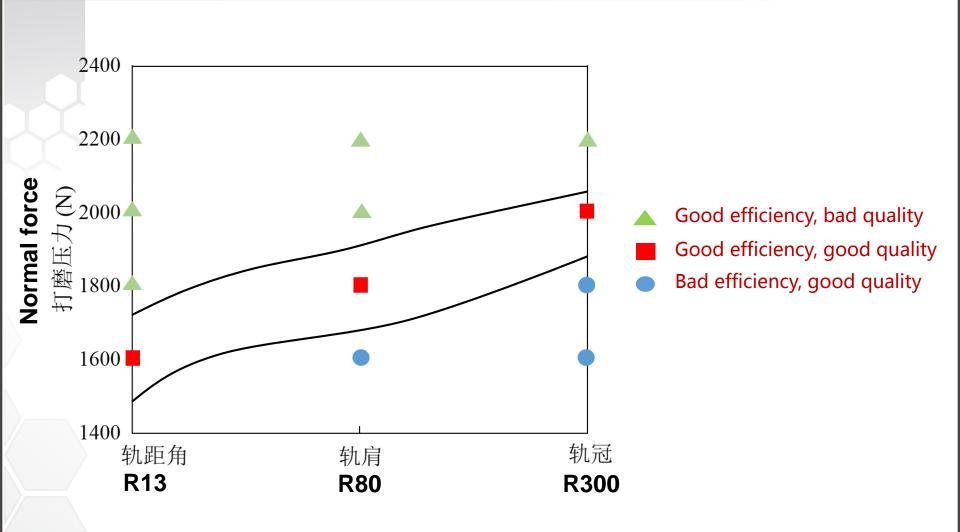
1600N

1800N

2000N

2200N

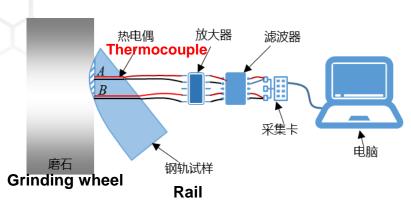


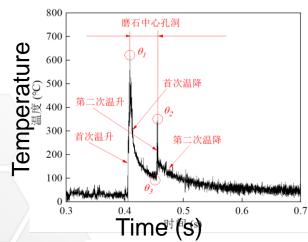




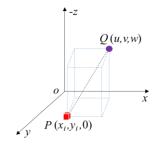
Grinding heat

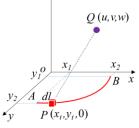
Experiments





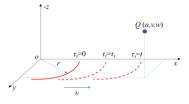
Numerical calculation

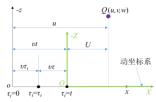




$$d\theta = \frac{q_l dl}{c\rho (4\pi\alpha\tau)^{3/2}} e^{\frac{(u-x_l)^2 + (v-y_l)^2 + w^2}{-4\alpha\tau}}$$

$$d\theta = \frac{q_l dl}{c\rho (4\pi\alpha\tau)^{3/2}} e^{\frac{(u-x_l)^2 + (v-y_l)^2 + w^2}{4\alpha\tau}} \qquad \theta = \int_{y_l}^{y_2} \frac{q_l}{c\rho (4\pi\alpha\tau)^{3/2}} e^{\frac{(u-\sqrt{r^2-y^2})^2 + (v-y)^2 + w^2}{4\alpha\tau}} \sqrt{1 + \frac{y^2}{r^2-y^2}} dy$$



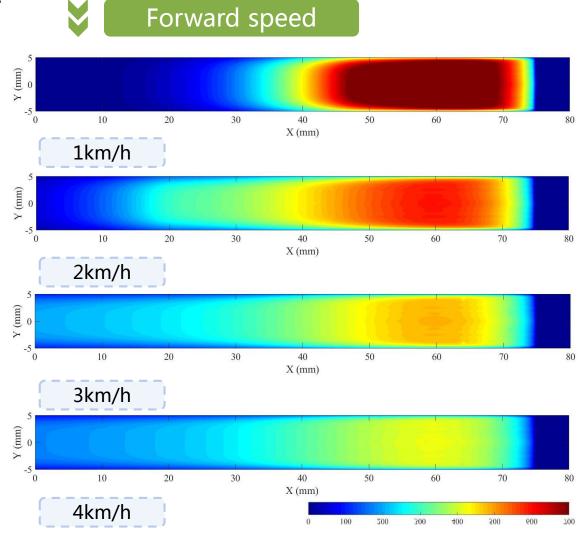


$$\theta = \int_{0}^{t} \int_{y_{1}}^{y_{2}} \frac{q_{1}}{c\rho \left(4\pi\alpha\tau\right)^{3/2}} e^{\frac{\left(U+v_{o}\tau-\sqrt{r^{2}-y^{2}}\right)^{2}+\left(V-y\right)^{2}+W^{2}}{4\alpha\tau}} \sqrt{1+\frac{y^{2}}{r^{2}-y^{2}}} dld\tau$$

$$\theta = \int_{R_1}^{R_2} \int_0^r \int_{y_1}^{y_2} \frac{q_r}{c\rho (4\pi\alpha\tau)^{3/2}} e^{\frac{(U + v_m r - \sqrt{r^2 - y^2})^2 + (V - y)^2 + W^2}{4\alpha\tau}} \sqrt{1 + \frac{y^2}{r^2 - y^2}} dld\tau dr$$

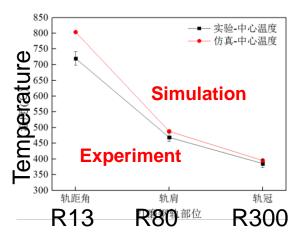


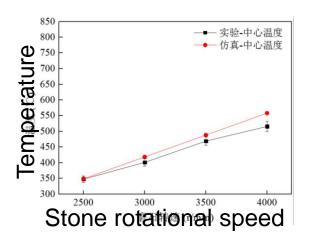
Grinding heat

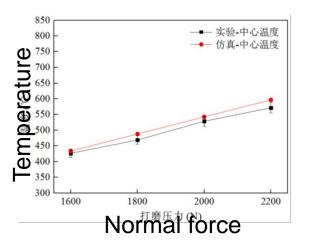


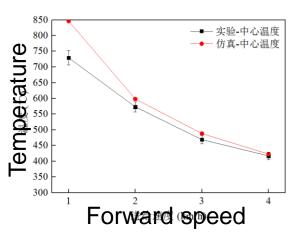


Grinding heat



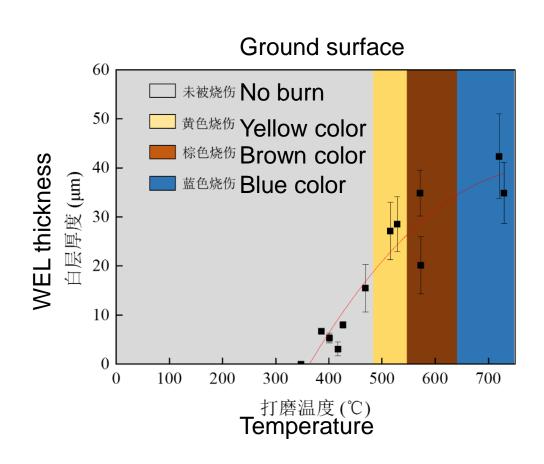








Grinding heat



Temperature vs. WEL thickness



1. Wear and RCF of wheel/rail under complex environment

- Low temperature: brittleness & RCF /
- Windblown sand condition : CoA & Wear >

2. Microstructure evolution of wheel/rail materials

3. Wear and RCF prediction

- Wear rate-Ty/A
- Shakedwon map

4. Rail grinding

Grinding parameters VS. grinding efficiency and quality



Thank you for your attention!

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