# **BHP**

# Case study: Turnout performance under heavy haul traffic – challenges and initiatives

#### Simone Issomura

ICRI Workshop August 27, 2023 - Rio de Janeiro





### Introduction

**Simone Issomura MEng** 

Senior Track and Civil Engineer BHP

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Simone Issomura was born in Brazil, great-granddaughter of Japanese immigrants. She received her Construction Technician degree in 1999 and Civil Engineering Bachelor's degree in 2004.

She started her railway career at São Paulo Subway's Permanent Way Department in 2006, while studying Quality and Reliability Engineering concurrently, in a specialisation course. After that she wrote a monograph about alternatives to minimise turnout wear as part of a specialisation course in Railway Engineering.

She worked on railways that mixed passenger, general cargo and heavy haul traffic, in areas such as Track Reliability, Turnout Renewals and Corporative Rail Engineering.

Simultaneously she was completing her Master's degree in Transport Engineering where she analysed heavy haul turnout components' performance in her dissertation.

Simone left Brazil as a Senior Engineer and moved to Australia in 2019. She worked supporting the turnout maintenance teams in the Pilbara region, and finally joined BHP's Rail Engineering Track and Civil team in 2021.

Altogether Simone has had 17 years of experience in railways, in Brazil and Australia. She is passionate about combining theory and practice to develop engineering initiatives that improve safety, efficiency, productivity, cost-benefit and reliability.



# 1. Objective



# **Objective**

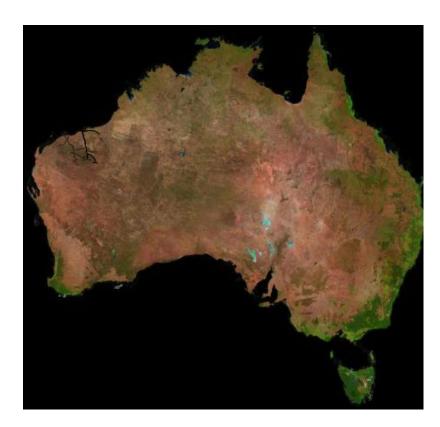
To present some challenges and initiatives related to turnout performance under heavy haul traffic.



# 2. Introduction



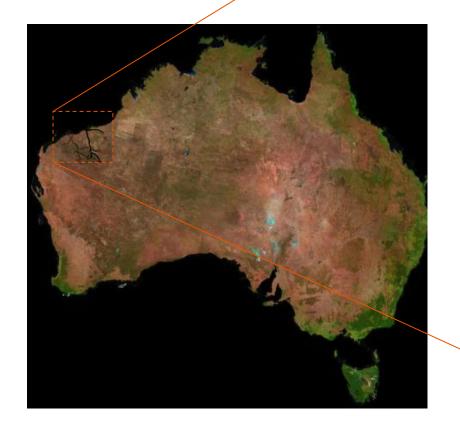
### **The BHP Network**



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## **The BHP Network**









#### **Features:**

Gauge = 1435mm

Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

#### **Features:**

Gauge = 1435mm

Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

Turnout design:

Rate

1:10 R221m



#### **Features:**

Gauge = 1435mm

Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

Turnout design:

Rate



1:10 R221m

1:15 R320m

#### **Features:**

Gauge = 1435mm

Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

Turnout design:

Rate

1:10 R221m



1:15 R320m



1:20 R910m



#### **Features:**

Gauge = 1435mm

Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

#### Turnout design:

Rate





1:15 R320m



1:20 R910m



**1:20 R1000m (tangential)** 



#### **Features:**

Gauge = 1435mm

Axle load = 40t

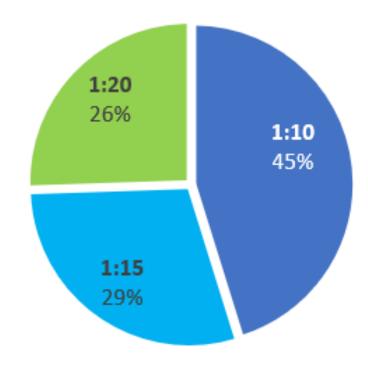
Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

#### Turnout design:

Rate





#### **Features:**

Gauge = 1435mm

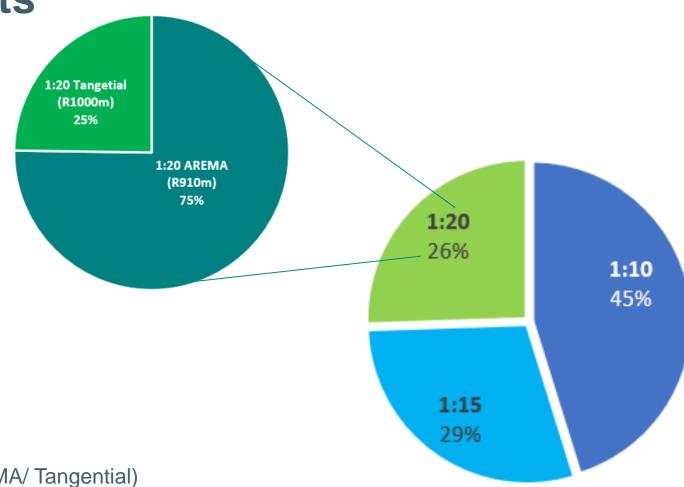
Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

- Rate
- Geometry (AREMA/ Tangential)





#### **Features:**

Gauge = 1435mm

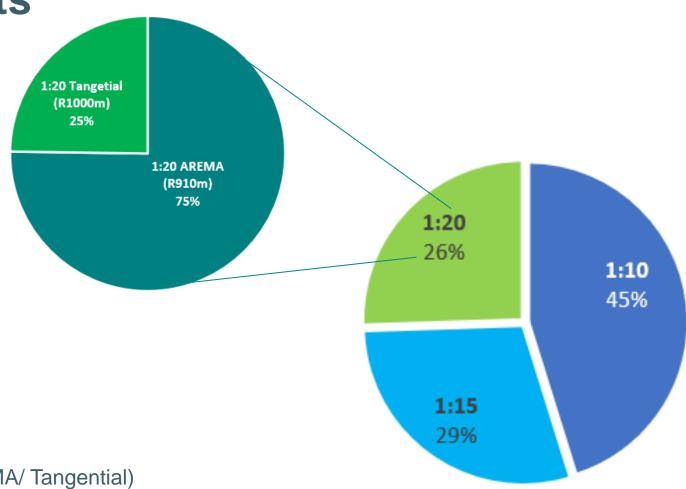
Axle load = 40t

Cargo = iron ore

Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

- Rate
- Geometry (AREMA/ Tangential)
- Frogs





#### **Features:**

Gauge = 1435mm

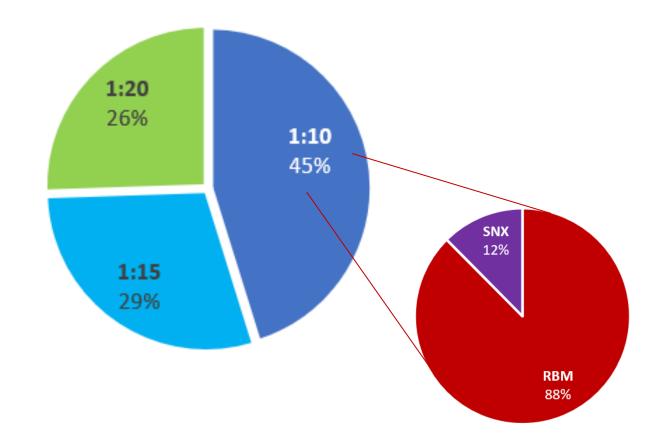
Axle load = 40t

Cargo = iron ore

#### Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

- Rate
- Geometry (AREMA/ Tangential)
- Frogs





#### **Features:**

Gauge = 1435mm

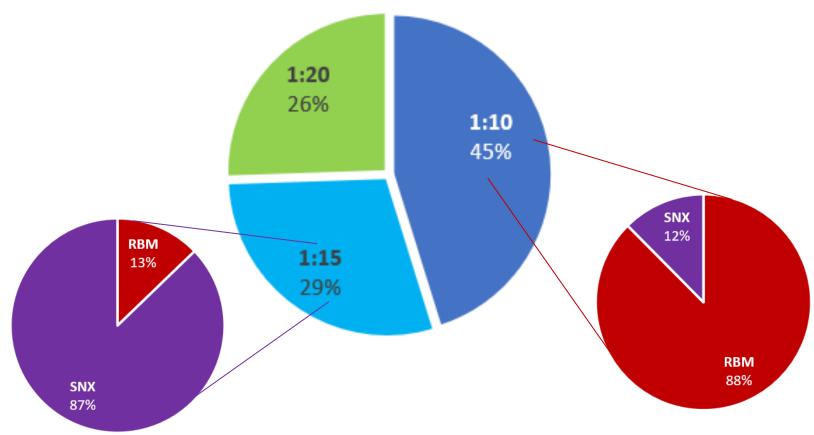
Axle load = 40t

Cargo = iron ore

#### Diverge design speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

- Rate
- Geometry (AREMA/ Tangential)
- Frogs





#### **Features:**

Gauge = 1435mm

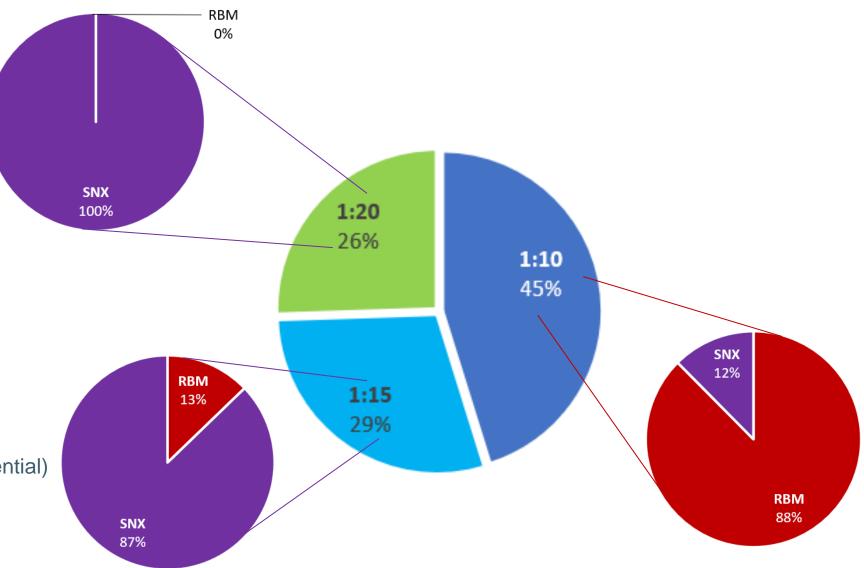
Axle load = 40t

Cargo = iron ore

#### Diverge Speed:

- 1:10 30km/h
- 1:15 35km/h
- 1:20 65km/h

- Rate
- Geometry (AREMA/ Tangential)
- Frogs





# 3. Challenges

Wear



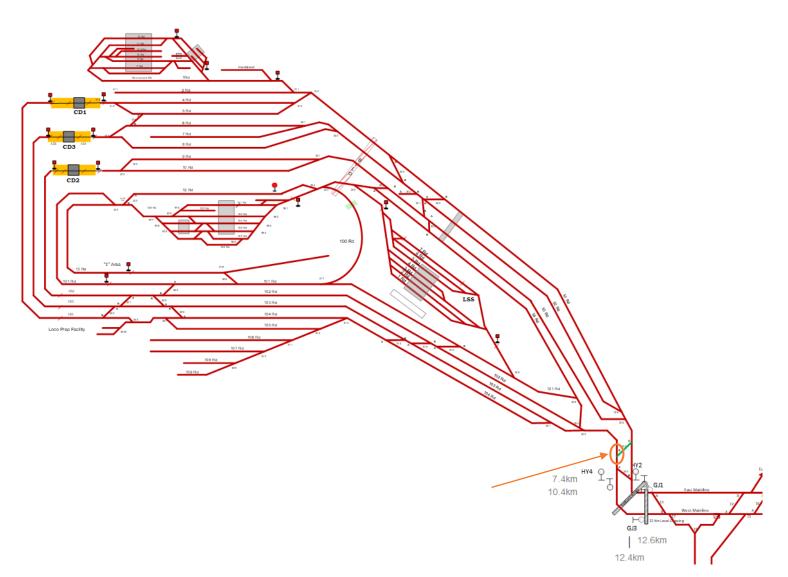
#### Wear

Example: 1:15 AREMA curved blade

Install date: 13/03/2023

Replace date: 16/07/2023

Life in service: 125 days





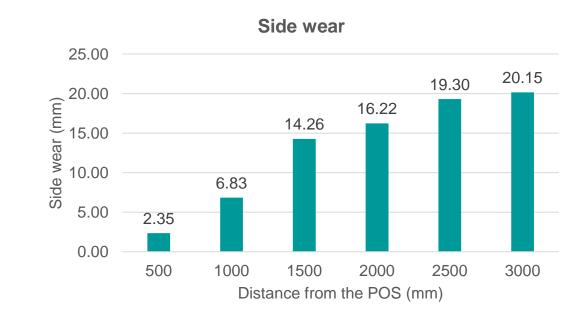
#### Wear

Example: 1:15 AREMA curved blade

Install date: 13/03/2023

Replace date: 16/07/2023

Life in service: 125 days





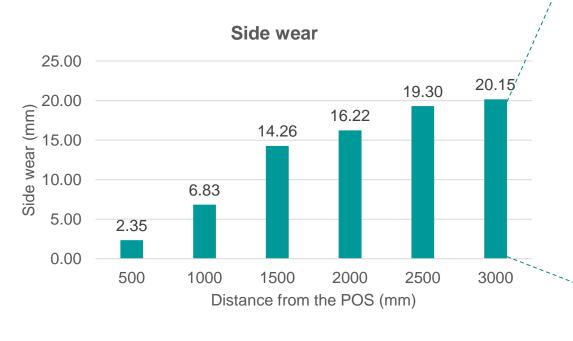
#### Wear

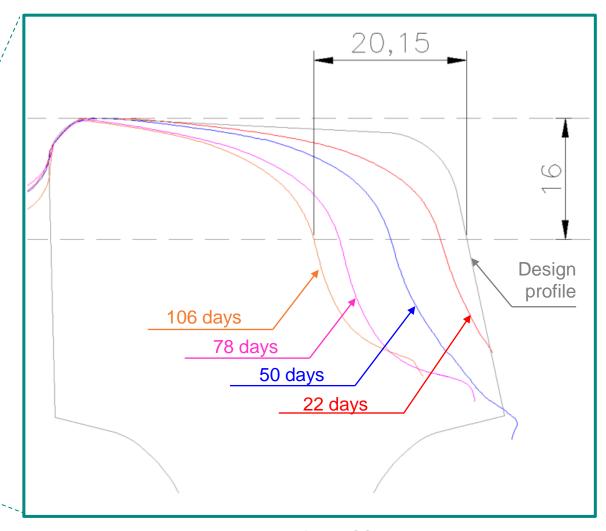
Example: 1:15 AREMA curved blade

Install date: 13/03/2023

Replace date: 16/07/2023

Life in service: 125 days





1:15 turnout - curved blade - 3000mm from POS



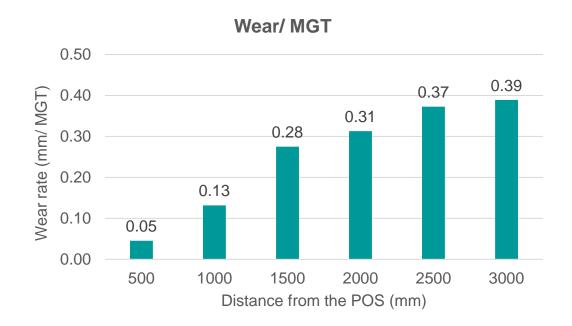
#### Wear

Example: 1:15 AREMA curved blade

Install date: 13/03/2023

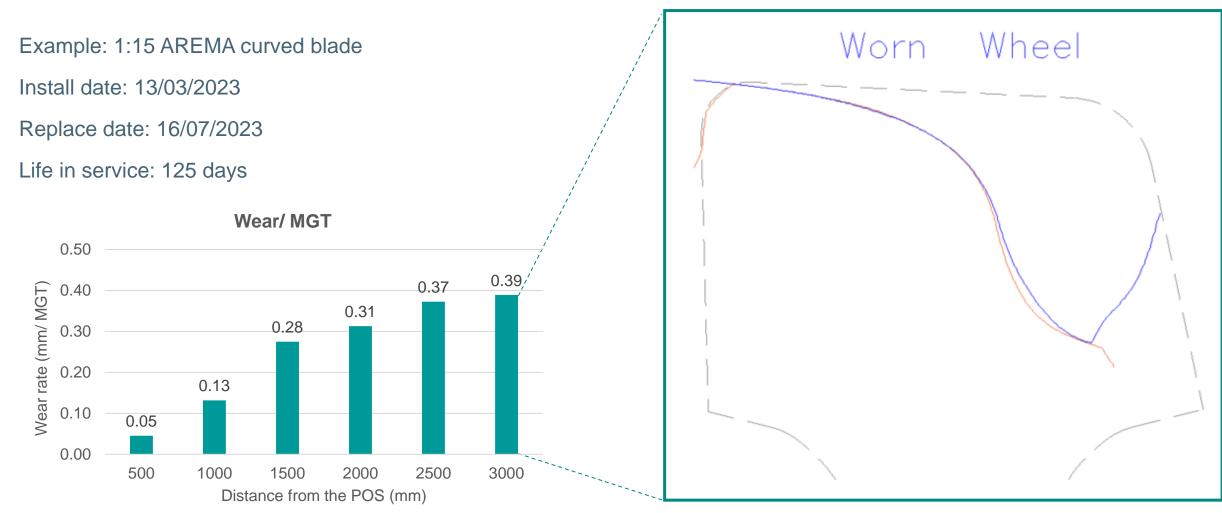
Replace date: 16/07/2023

Life in service: 125 days





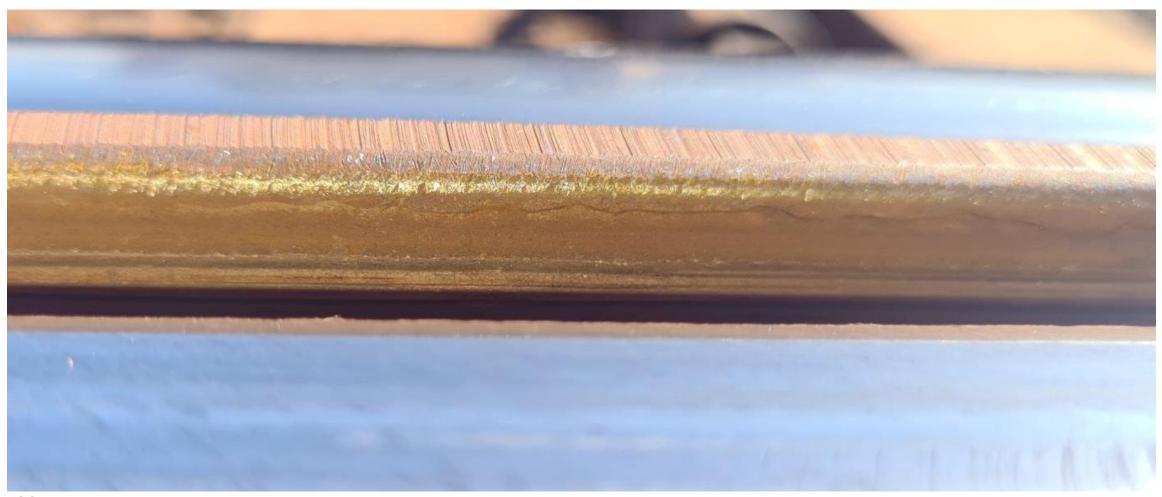
#### Wear



1:15 turnout – curved blade – 3000mm from POS and a worn wheel



**Switch blade defects – Field Side Cracking (FSC)** 



FSC – Initial stages



**Switch blade defects – Field Side Cracking (FSC)** 

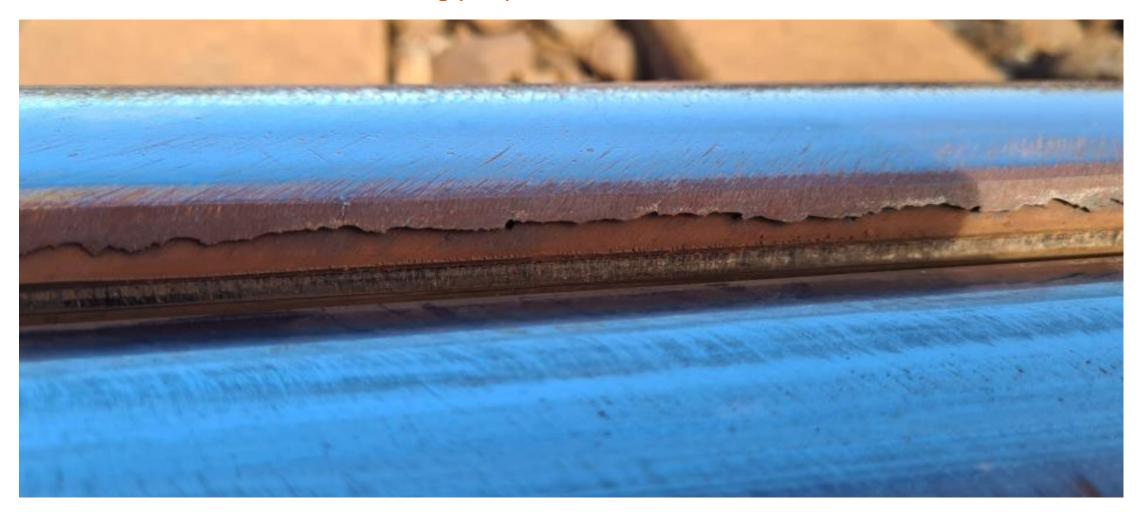
Different depths





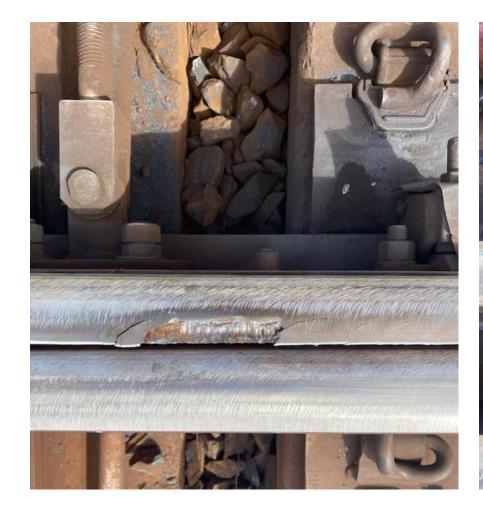
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**Switch blade defects – Field Side Cracking (FSC)** 





**Switch blade defects – Field Side Cracking (FSC)** 

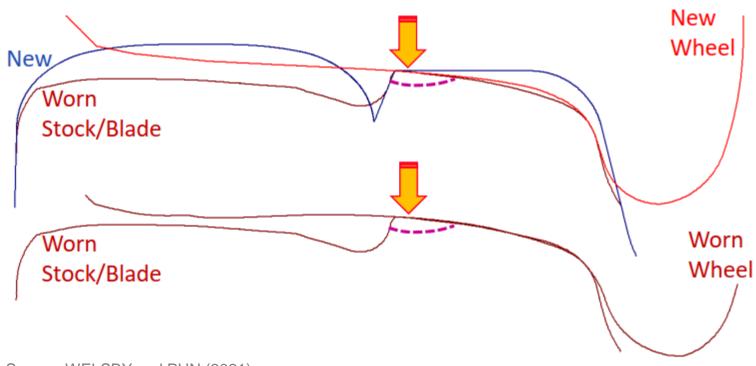






#### **Findings**

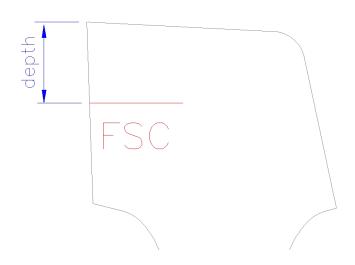
The new and less worn wheels contact sits on top of the field side edge of blade, causing extreme contact stresses and subsurface shear stresses.

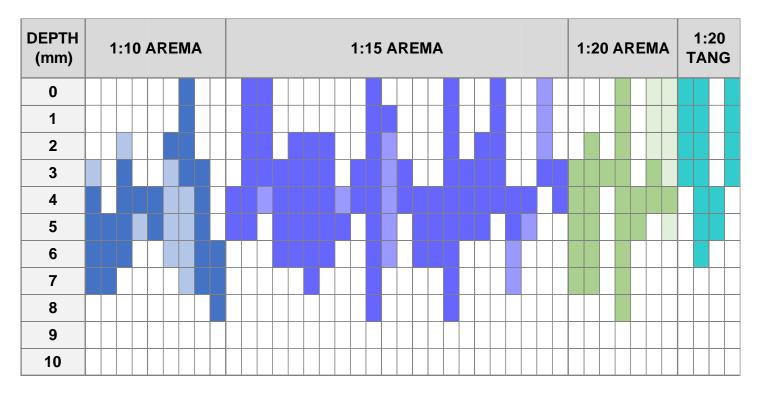


Source: WELSBY and PUN (2021)



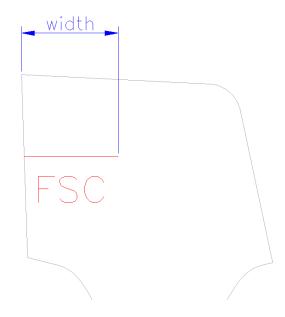
**FSC** development – depth

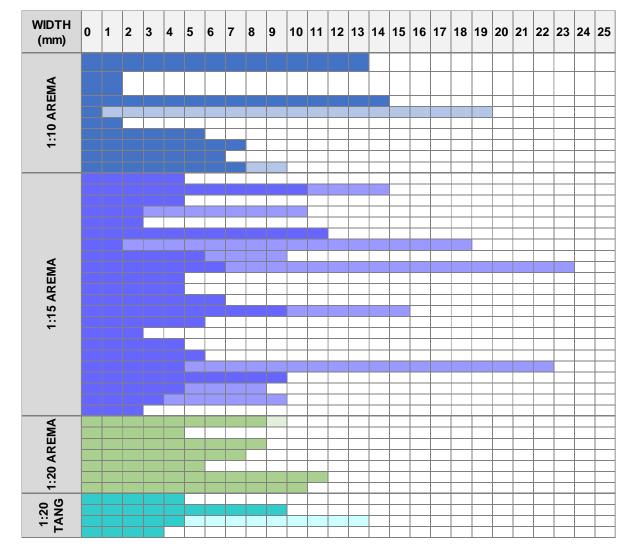




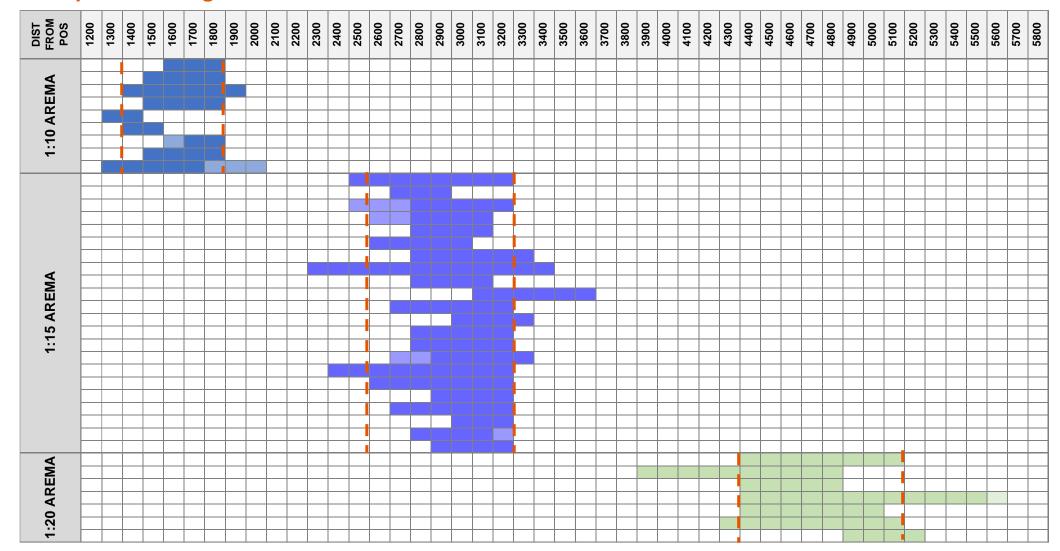


**FSC** development – width

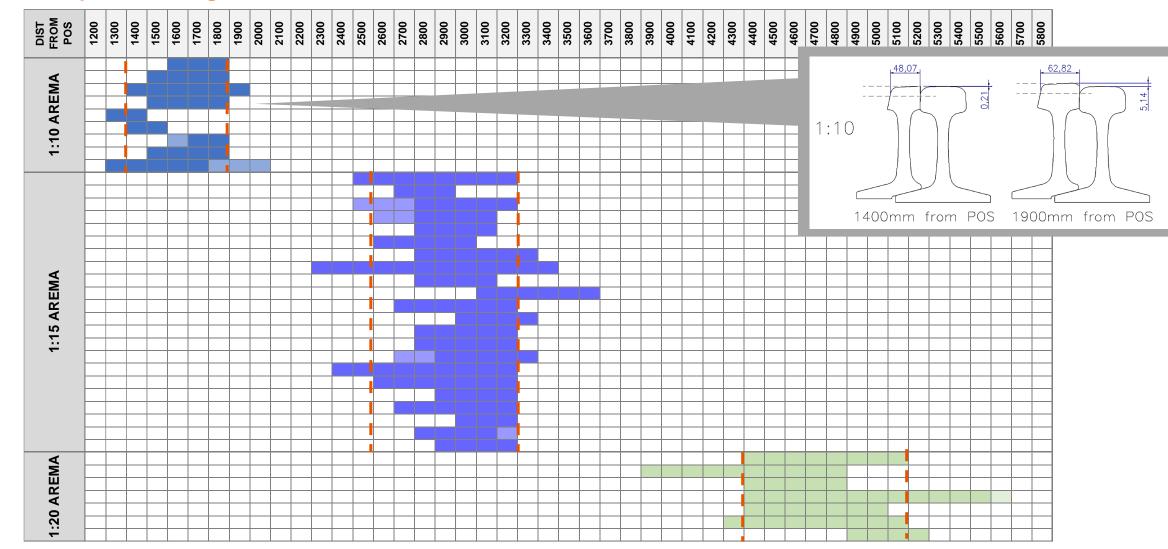




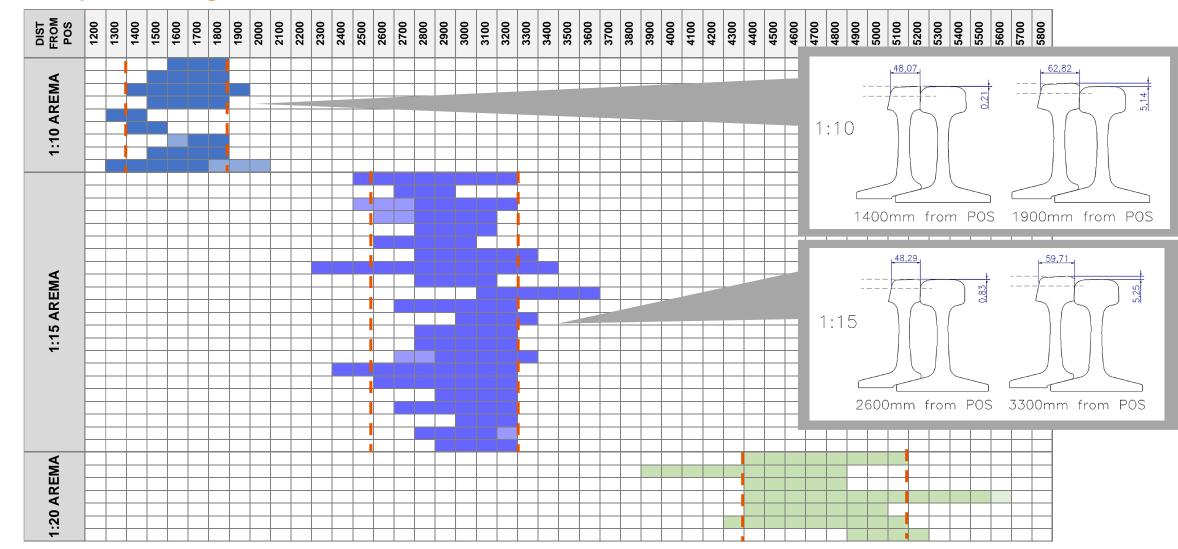




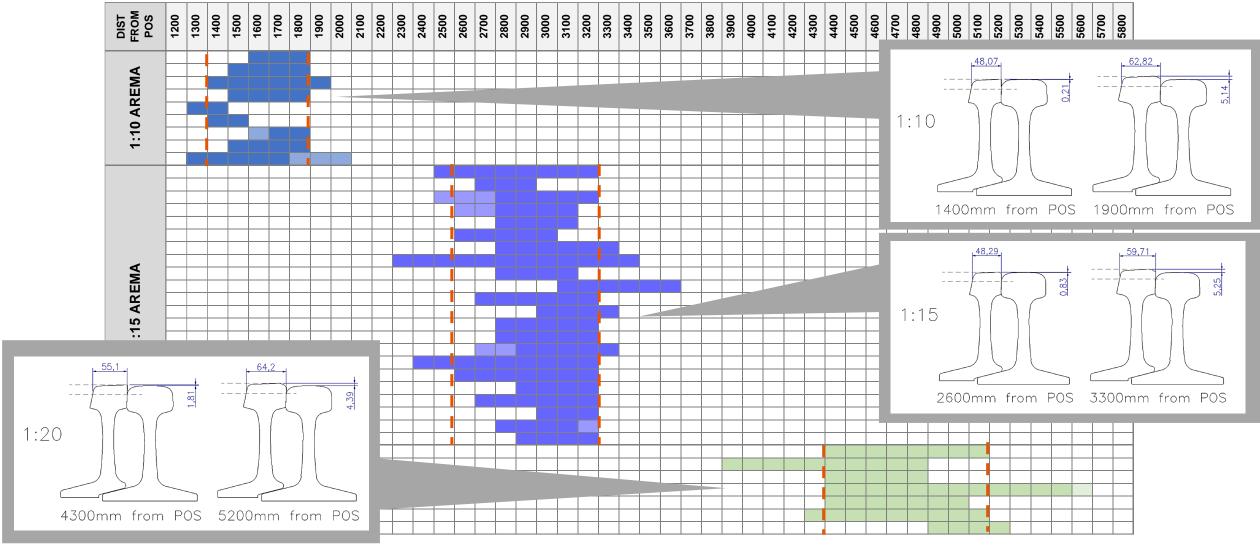




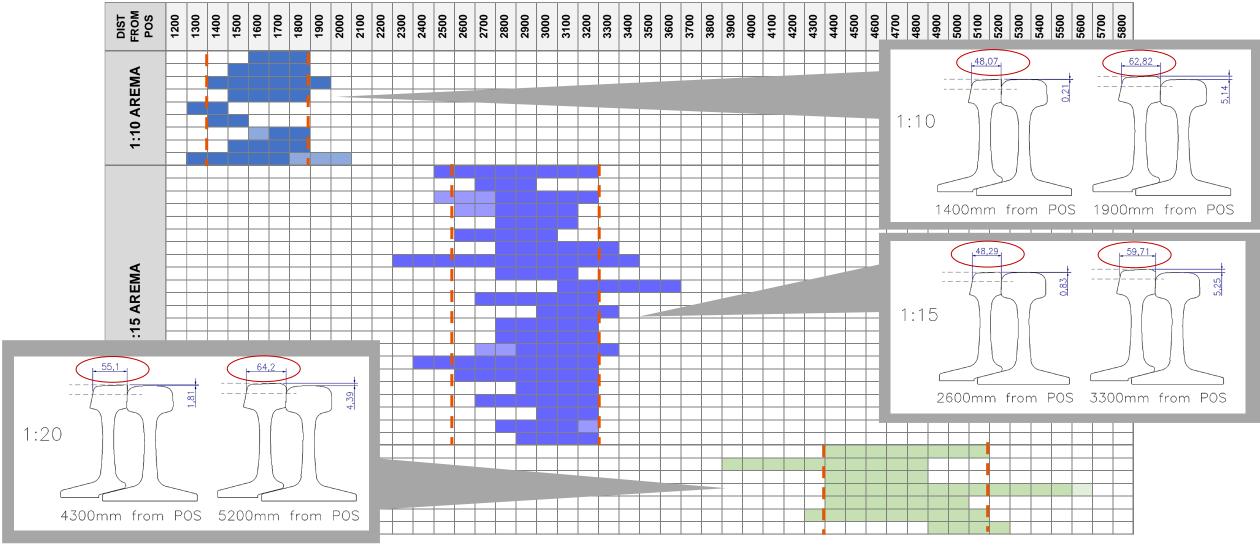




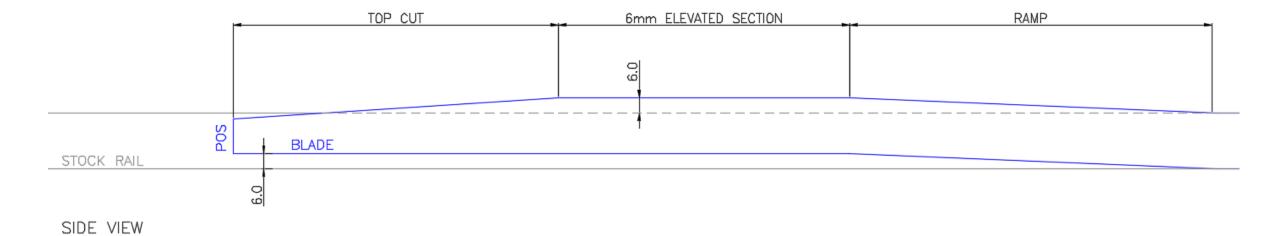




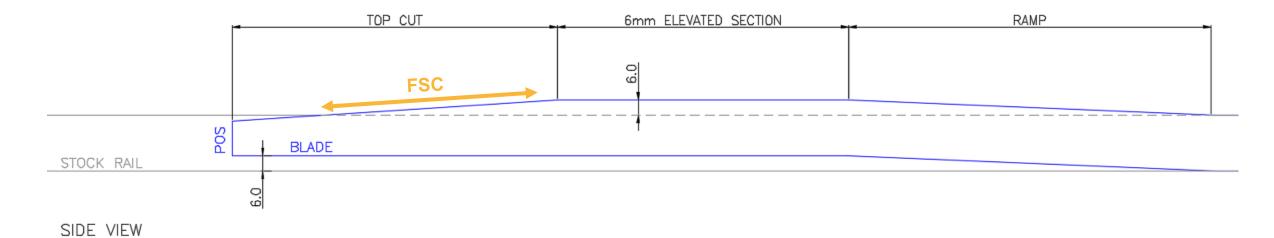




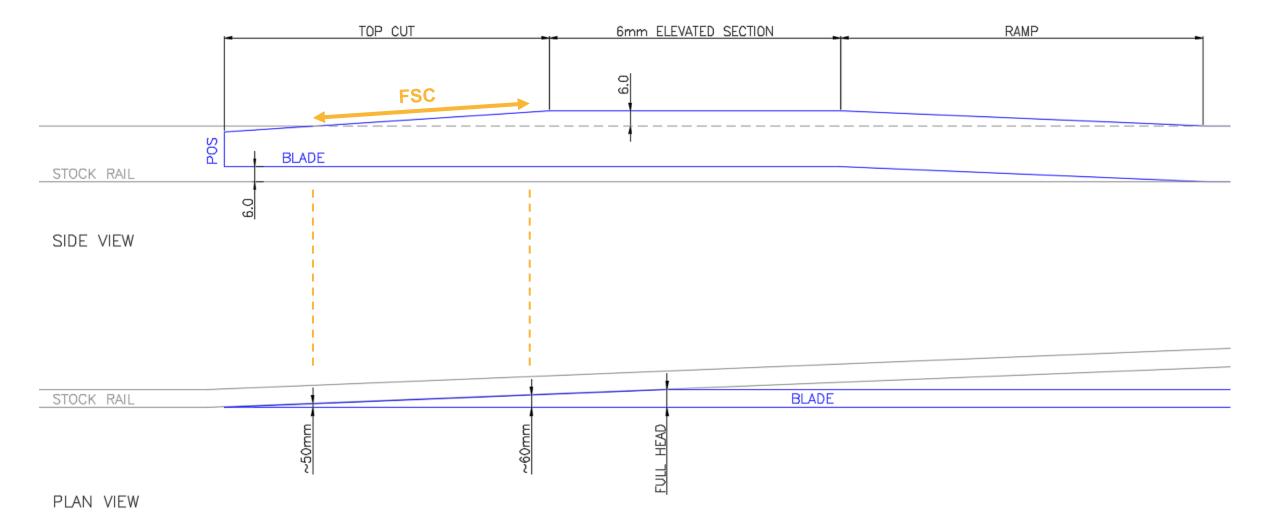




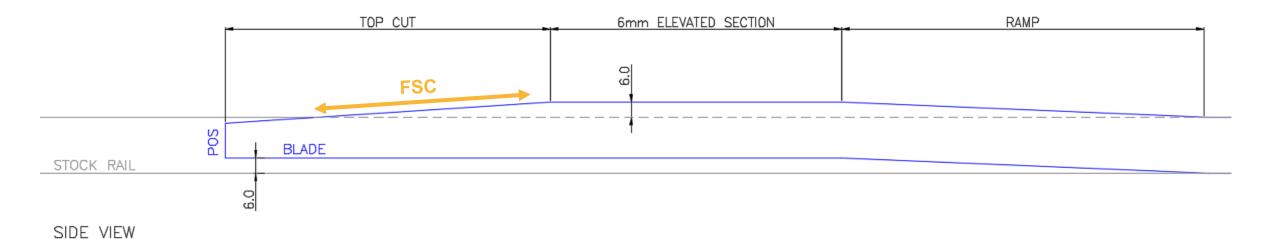












Turnout rate	SR&B same level	FSC	zone	Top cut end	6mm elevated section end	Ramp end
	from POS (mm)	from	to	from POS (mm)	from POS (mm)	from POS (mm)
1:10	1551	1400	1800	2133	3276	4343
1:15	2660	2600	3300	3658	6376	8459
1:20	4790	4300	5100	6096	9250	11350



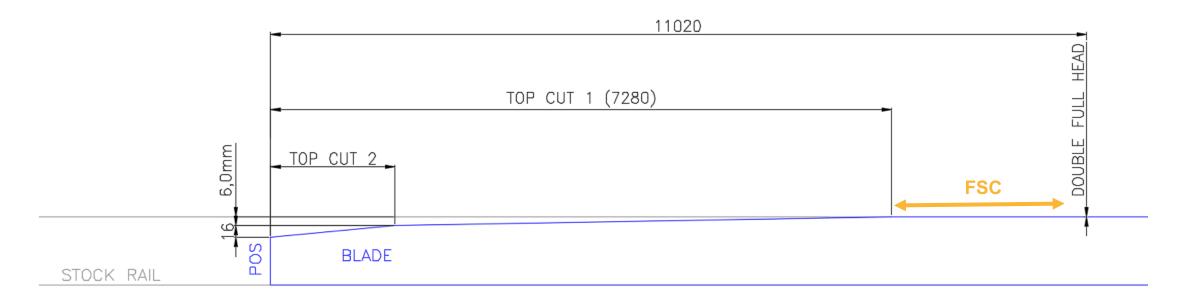
# Turnouts performance FSC development - Length

DIST FROM POS	7000	7100	7200	7300	7400	7500	7600	7700	7800	7900	8000	8100	8200	8300	8400	8500	8600	8700	8800	8900	0006	9100	9200	9300	9400	9500	9	9200	80	0066	000	910	ŏ	10300	10400	10500	10600	10700	10800	10900	11000
1:20 TANG																																									



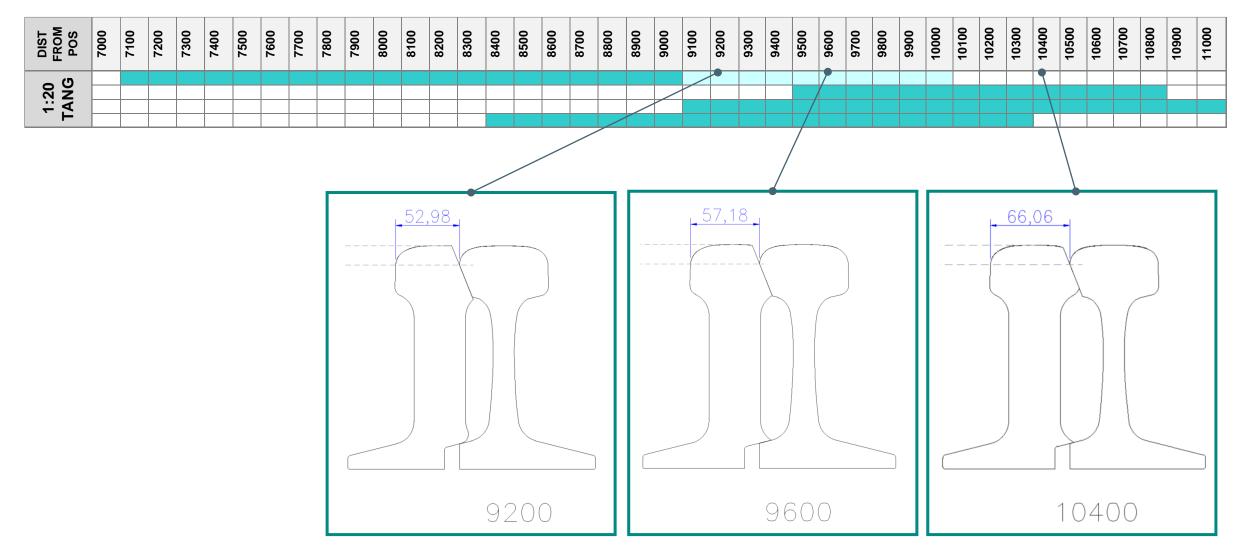
**FSC** development – Length

DIST FROM POS	7000	7100	7200	7300	7400	7500	2600	7700	7800	7900	8000	8100	8200	8300	8400	8500	8600	8700	8800	8900	0006	9100	9200	9300	9400	9200	0096	9700	9800	0066	10000	10100	10200	10300	10400	10500	10600	10700	10800	10900	11000
1:20 TANG																																									



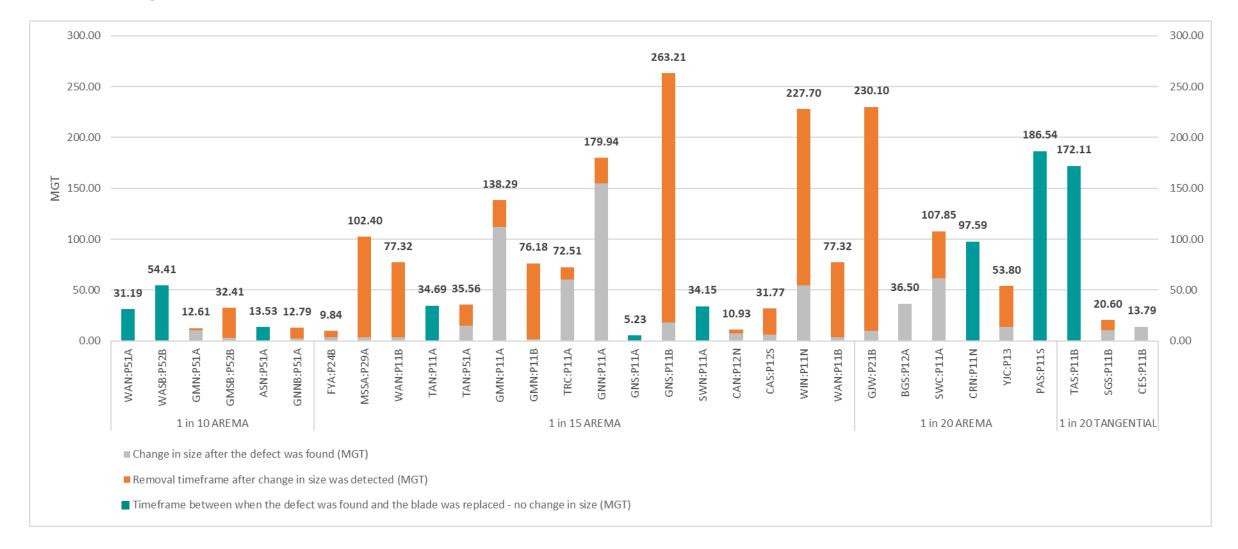
SIDE VIEW





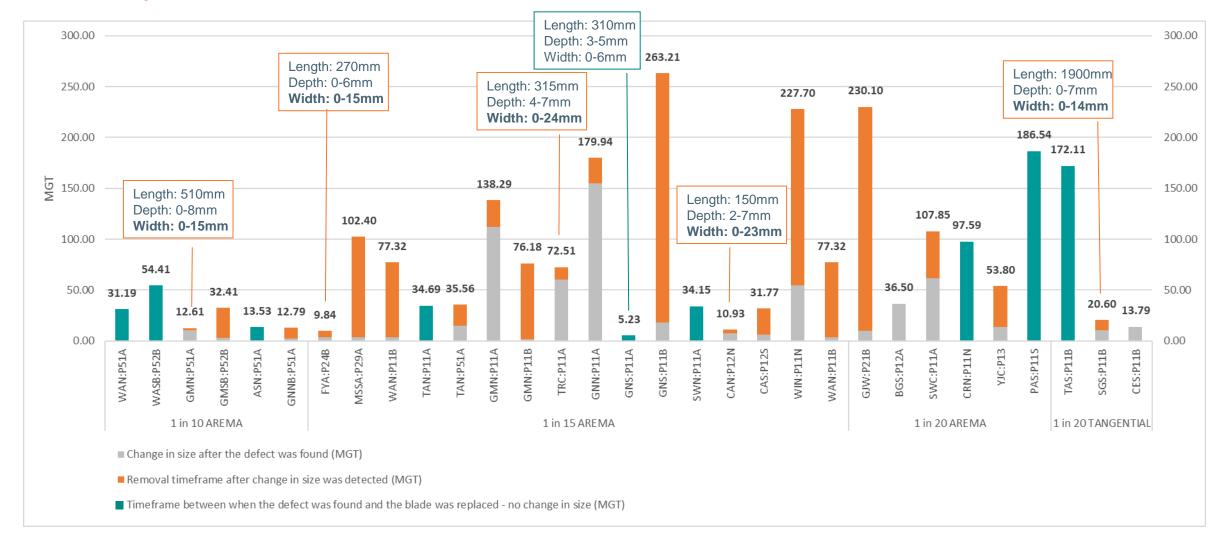


### **FSC** development





### **FSC** development





### **FSC** development





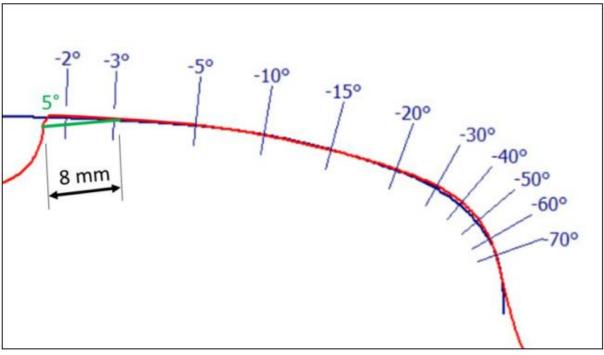
### **Work Instruction**

# Work instruction 0173018 – Grinding to Prevent Field Side Cracking in Switch Blades

Grind a single 5° facet up to 8mm wide along the field edge.

Higher angles remove material support and can result in more rapid flow development.

Care must be taken not to impact the stock rail during grinding.

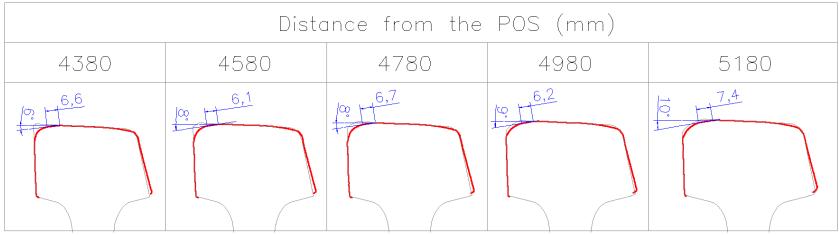


Source: Work Instruction 0173018 - Grinding to Prevent Field Side Cracking in Switch Blades

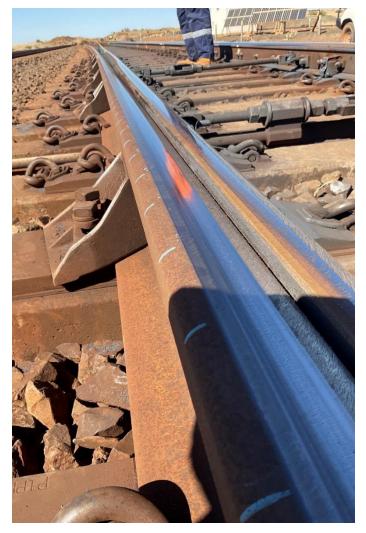


### Hand grind – 1:20 AREMA turnout

Profile measurements were taken after grinding to check compliance to the Work Instruction



Profile measurements from a 1:20 AREMA turnout – after hand grinding

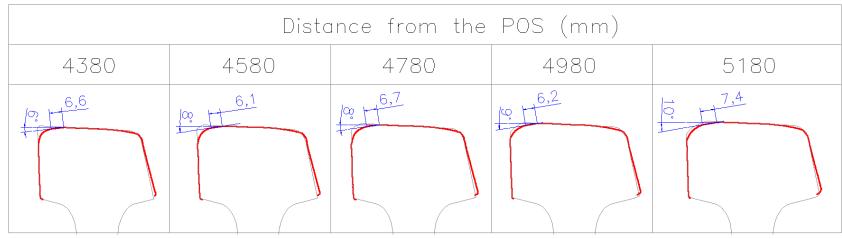


1:20 AREMA turnout



### Hand grind – 1:20 AREMA turnout

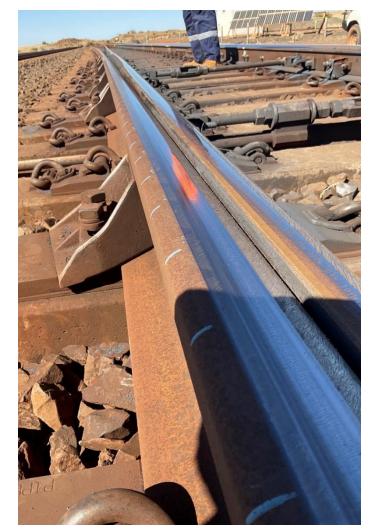
Profile measurements were taken after grinding to check compliance to the Work Instruction



Profile measurements from a 1:20 AREMA turnout – after hand grinding

### Next steps:

- Protractor to be used
- · Customised gauge to be designed
- Management of stock rail and blade differential height



1:20 AREMA turnout



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Profile measurements were taken before and after grinding on both blades to check compliance to the Work Instruction



Profile measurements were taken before and after grinding



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – before grinding



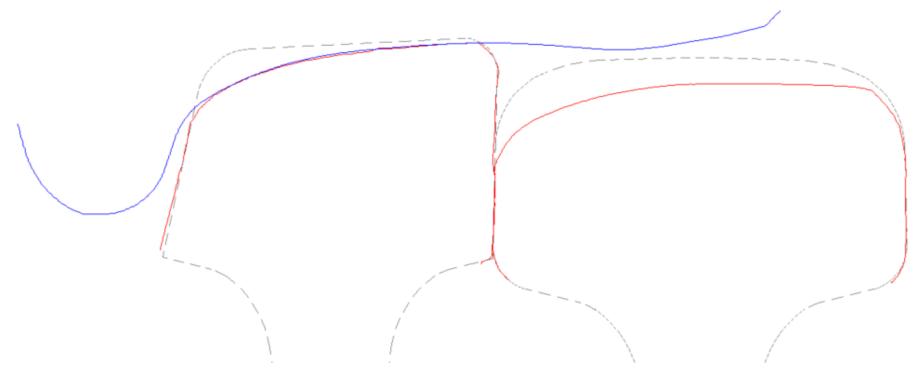
RH Blade, No. 5 = 3000mm from POS

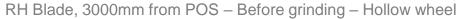


### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – before grinding

# 1.2 Hollow

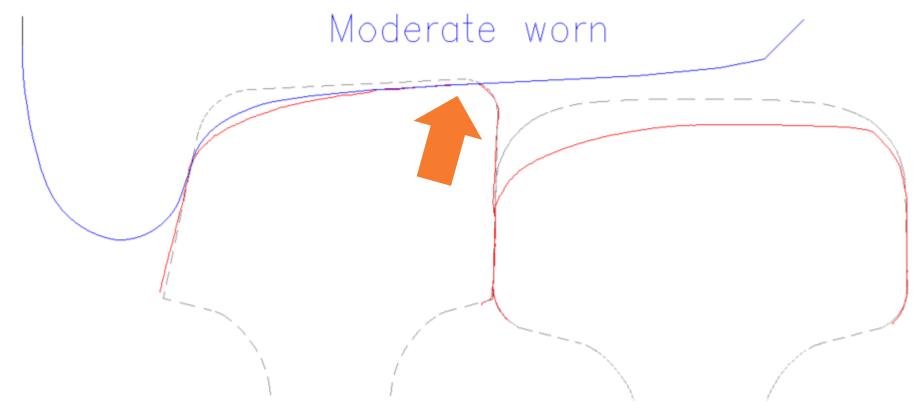






### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – before grinding

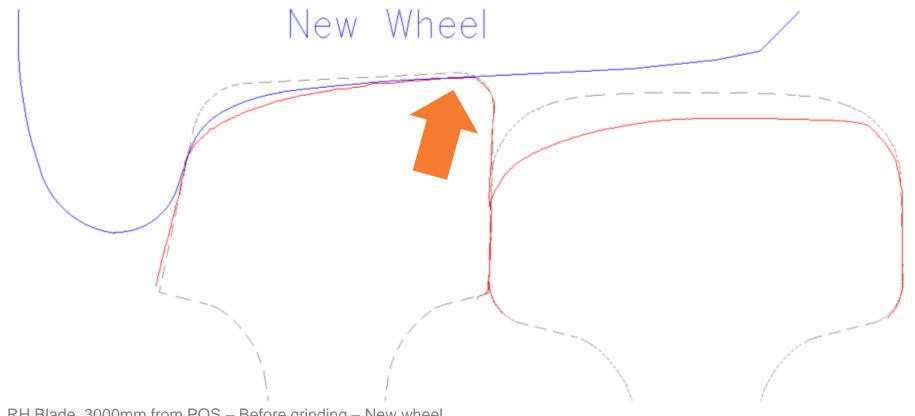


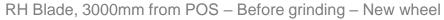
RH Blade, 3000mm from POS – Before grinding – Moderate worn



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – before grinding

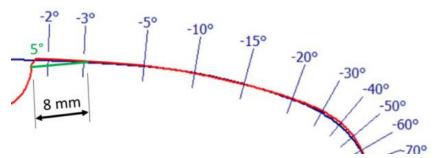






### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Profile measurements taken after grinding



		n D L	Distance	e from the	e POS (mr	n)	
	-200	2250	2500	2750	3000	3250	3500
RH	1,3 80 7	A: 10; ===	15. 7.6 7.6	/br 7.5	15. 8,4 12. 8,4	6,5	6, 9,2
LH	16 4,3	3.32	9,6	A: 8,2	3:13:6	Con the control of th	10,6

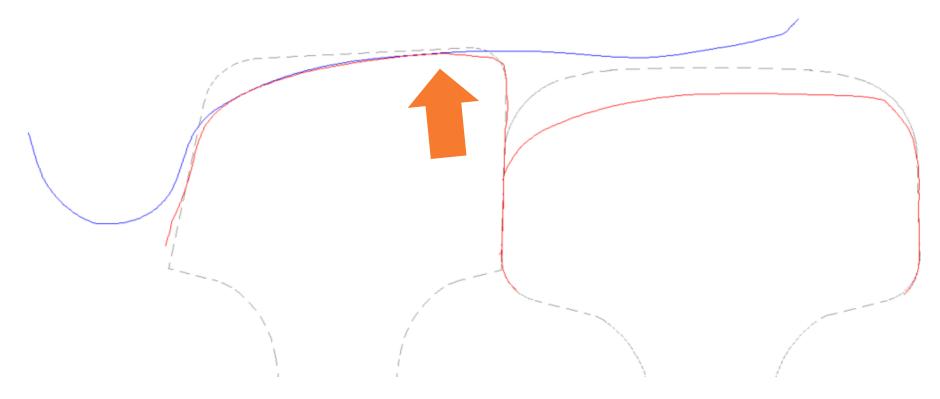
Profile measurements after grinding



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – after grinding

# 1.2 Hollow

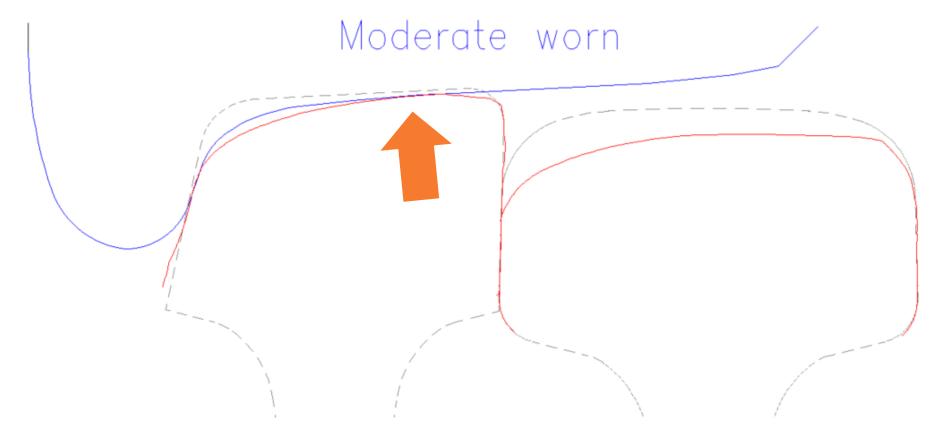


RH Blade, 3000mm from POS – After grinding – Hollow wheel



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – after grinding

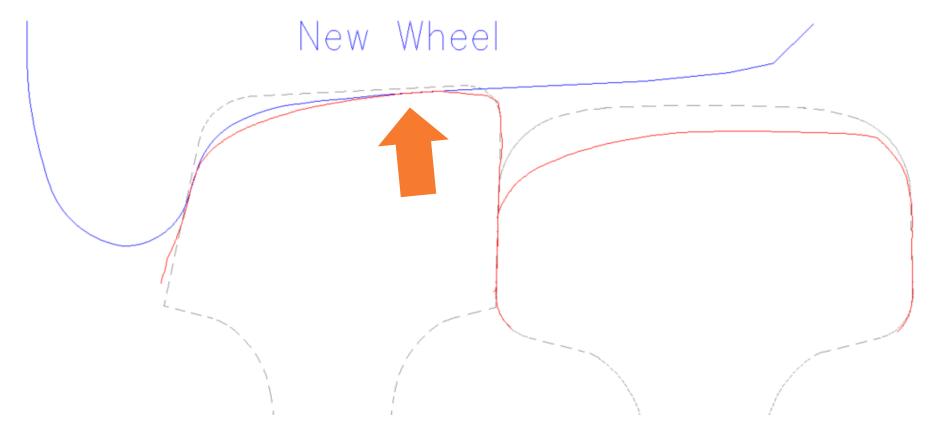


RH Blade, 3000mm from POS – After grinding – Moderate worn wheel



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

Example: profile measurement taken at 3000mm from POS – after grinding



RH Blade, 3000mm from POS – After grinding – New wheel



### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout

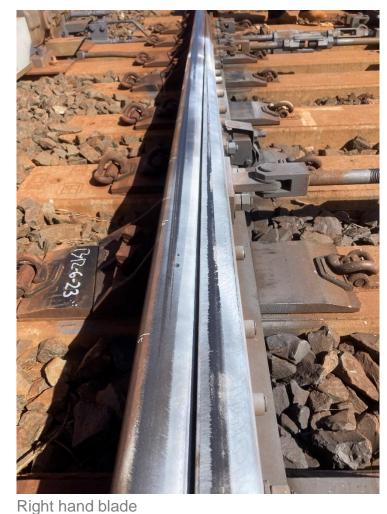




Right hand blade

Left hand blade

### Trial at Chichester Backtrack – 1:15 AREMA RH Turnout





de Left hand blade

### Next steps:

- Monitor and if successful, include it in the Maintenance Strategy
- Optimise the turnout design implementing the 5 degrees facet from the manufacturing stage



### **Pre-Profiling Project**



### Main goals:

- 1) Increase safety
- 2) Increase the performance of the turnout components and wheels
- 3) Reduce track time to implement the desired profiles
- Develop maintenance strategy and support to control defects and prevent failures

Proposed profiles (trial) – initial verification



### **Pre-Profiling Project**



Proposed profiles (trial) – initial verification

### Main goals:

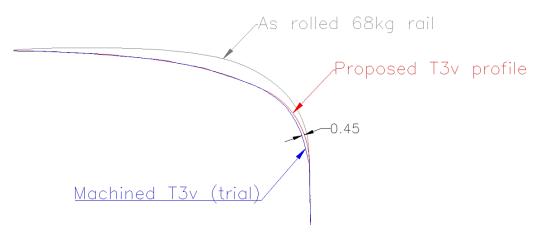
- 1) Increase safety
- 2) Increase the performance of the turnout components and wheels
- 3) Reduce track time to implement the desired profiles
- Develop maintenance strategy and support to control defects and prevent failures

### **Initial analysis:**

- 1) Existing turnouts and wheels' performance analysis
- Simulate wheel-rail impact loading under new and worn turnouts and wheel profiles
- 3) Simulate wheel-rail contact dynamically under different conditions (new/moderate worn/hollow wheels, new/worn rails, facing/trailing directions, straight/reverse routes)
  - a) Propensity for wear, plastic deformation and RCF development
  - b) Flange climb risk



### **Pre-Profiling Project**



Comparison between proposed and machined profiles

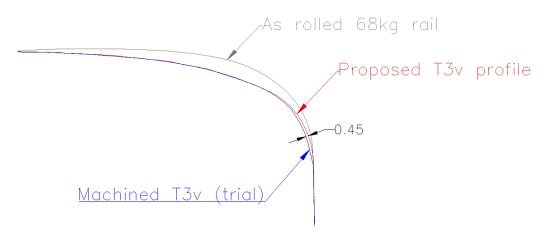


### **New turnout profiles:**

- 1) Customise and optimise the wheel-rail contact
- 2) Re-simulate
- 3) Modelling



### **Pre-Profiling Project**



Comparison between proposed and machined profiles



### **New turnout profiles:**

- 1) Customise and optimise the wheel-rail contact
- 2) Re-simulate
- 3) Modelling

### **Next Steps:**

- 1) Finalise the stock rail and blade analysis
- 2) Re-assess the whole turnout set after modelled
- 3) Manufacture
- 4) Trial
- 5) Monitor and validate
- 6) Amend and re-simulate, if necessary
- 7) Implementation
- 8) Training, tools, development of maintenance thresholds and strategy to control defects and failure prevention



# 5. Conclusion



# In conclusion

Turnouts increase the railway system's capacity, providing strategic and operational flexibility. On the other hand, the desired operational excellence in heavy haul railways requires constant and proportional investment to match the efficiency challenges (such as the increase in train size, speed, axle load and headway reduction) with the permanent way capacity.

The trials and initiatives to enhance the turnouts' performance are only possible due to the continuous improvement processes, which requires synergy, engagement and partnership among all parties (Maintenance, Track Inspectors, Grinding, Reliability, Engineering, the Manufacturer and the Institute of Railway Technology).



# Acknowledgement

I would like to thank all my railways colleagues that took or are taking part in this learning journey of discovery with me.





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# References

- Work Instruction 0173018 Grinding to Prevent Field Side Cracking in Switch Blades
- D. Welsby, J. Pun. Turnout Profiling and Management. Monash Institute of Rail Technology. 1st February, 2021



# Thank you!

**Simone Issomura MEng** 

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